Journal of Applied Geology Summer 2013, Vol. 9, No. 2: 169-175 www.appliedgeology.ir



Improve of rubber physical properties with addition of waste calcium carbonate

A. Esmaili Mahani^{*1} & M. H. Azadi²

1) University Lecturer, Department of Mining Engineering, Neyriz Branch, Islamic Azad University, Neyriz, Iran, esmaili235@gmail.com

2) Ph.D Student and Member of Young Researchers club, Shiraz Branch, Islamic Azad University, Shiraz, Iran,

mh.azadi_g@yahoo.com *) Correspondence Author

Received: 5 Jul. 2012; revised: 23 Jun. 2013; accepted: 25 Jun. 2013; available online: 6 Sep. 2013

Abstract

In the present study, the effects of waste calcium carbonate on properties of rubber were investigated. The rubber samples were prepared with weight percentage 15Wt% of waste calcium carbonate (four different samples), pressed in 4MPa and sintered at 1500C for 60 minutes. The properties such as hardness, elongation at rupture, tensile strength and 300% modulus were measured. The chemical analysis of calcium carbonate was investigated through X-Ray Fluorescence method (XRF) and sizing distribution of calcium carbonate were carried out through Laser Particle Size Analyzer device (LPSA). The results indicated that by increasing the waste calcium carbonate weight percentage up to 15Wt%, the physical properties of the rubbers improved. Also, more increasing the waste calcium carbonate led to decrease in favorable properties and standard.

Key words: rubber, waste calcium carbonate, additive, physical properties.

1. Introduction

Calcium carbonate (CaCO3) powder is a common filler in many industries, including in the rubber industry where it is used in the production of rubbers (Boynton 1980, Lefond 1983). Substituting a small percentage (3-5%) of the carbon black in a rubber with CaCO3 can decrease the rubber density and increase mechanical strength (by 40-45%), which increases its service life (Kauffman et al. 1974, Von Flotow & Etkin 1981, Bagghi & Sharma 1981, Gent 2001, Ai-lon 2012). Calcium carbonate is preferred over other fillers, such as barium sulfate (barite), aluminum silicate (kaolin), mica, pyrophyllite, silica, slate and magnesium silicate (talc) (Katz 1987), because it imparts softness, smoothness, resistance to abrasion, friction, erosion, and fire, and increases the flexibility and mechanical strength of the rubber (Poompradub 2010).Natural CaCO3 can be obtained from calcite and aragonite in mines. This CaCO3 can be found in limestone, spot disland, and other types of rock. Waste CaCO3 powder is produced as

a by-product in stone sawing factories with a typfical particle size of $0.5-1\mu m$ (Strutz & Sweeney 1990). CaCO3 powder can also be produced by reaction of carbon dioxide with calcium hydroxide. Ca(OH)2 + CO2 \rightarrow CaCO3

 Table 1. Properties of calcium carbonate (Bagghi &

 Sharma 1981, Richard & Lewis 2004)

CaCO3
White solid
Hexagonal, Orthrombic
1.658
100.09 gr
2.7 g/cm3
899 °C
825 °C

The precipitated CaCO3 has high purity (98–99%) and can be produced with a specific crystal morphology (Strutz & Sweeney 1990).

In this research, application of waste CaCO3 powder as a filler in rubber production was investigated.

Journal of Applied Geology, Summer 2013, Vol. 9, No. 2, 169

2. Experimental

2.1. Sample Collection

Samples were collected from stone sawing factories around Neyriz, Iran. There are about 175 stone sawing factories in this region, and all of them produce CaCO3 powder. Each factory produces about 10 t (1 t = 1000 kg) of pure and micronized CaCO3 powder daily, which could be used as a fillers in many industries.

2.2. Sample characterization

The samples were dried before analysis. Particle size analysis (PSA) (SALD-2101, Shimadzu, Kyoto, Japan, ISO/IEC 17025 standard) was conducted at the Pharmacological School of Shiraz University (Shiraz, Iran), and included measurement of the number of particles, and the longitudinal and surface area equivalent diameters of the particles. X-ray fluorescence (XRF) (PW 1480, Philips, Amsterdam, Netherlands) was used to determine 32 elements in the samples. This analysis was conducted at Kansaran Binaloud Labratory (Tehran, Iran). After analysis, the CaCO3 powder was used as a filler in production of rubber at Dena Tire Manufacturing Company (Shiraz, Iran). After weighing the basic raw materials for rubber production (Table 2), the material was mixed in a mill for 6 min, and curing agents and accelerators were added during this time. The compound produced was extruded through two rollers on the mill. Various grades of rubber compounds were produced, and used to manufacturer parts. The vulcanization was carried out in a hydraulic press under a pressure of about 4 MPa, temperature of 150°C for 60 minutes. In the final stage, the rubbers were formed and reached their maximum values for dynamic-mechanical properties and tensile strength. The rubbers were tested for hardness, tensile resistance, percentage of

elongation at rupture, and stress at 300% strain (300% modulus).

Table 2.	Composition	of	the	rubber	mixture	used	for
tire prod	uction						

Material	Proportion (g)			
Natural rubber (SMR 20)	100			
Oil (Behran 840)	8			
Stearic acid	2			
Black N_550 (reinforcement)	30			
ZnO2 powder	3.5			
(reinforcement -filler)	5.5			
Waste CaCO3 powder	15			
(reinforcement –filler)	15			
MBTS (accelerator)	0.4			
Sulfur (curing agent)	3			

3. Results and Discussion

3.1. Characterization of the CaCO3 powders

All four CaCO3 samples gave similar results for LPSA. Therefore, the results for only one of these samples are presented in this section. The particle size distribution (Figure 1) showed that the mean size was 0.597 μ m (range 0.365–35.701 μ m), the mode was 0.562 μ m, and the median was 0.561 μ m. Based on the longitudinal equivalent diameter (Figure 2), the mean particle size was 0.761 μ m (range 0.365–124.573 μ m), the mode was 0.562 μ m, and the median was 0.562 μ m, the mode was 0.562 μ m, and the median was 0.634 μ m. Based on the surface area equivalent diameter (Figure 3), the mean particle size was 1.925 μ m (range 0.365–188.947 μ m), the mode was 0.562 μ m, and the median was 1.281 μ m.

3.2. Chemical Analyses

The XRF results (Table 3) showed that the samples contained 0.17 % (Al2O3 + Fe2O3) and 0.35 % MgO on average.

	No.	CaO %	\$10 ₂ %	Fe ₂ O ₃	MnO %	MgO %	Al ₂ O ₃ %	K ₂ O %	Na ₂ O %	110 <u>2</u> %	2 F	² 05 %	L.O.I %
-	1	54.72	0.53	0.06	0.001	0.34	0.05	0.03	0.08	0.01	1 0	.067	43.66
	2	53.65	0.65	0.08	0.002	0.33	0.08	0.03	0.09	0.01) 0	.071	43.46
	3	54.32	0.56	0.15	0.001	0.39	0.07	0.03	0.14	0.00	3 0	.059	43.51
	4	54.31	1.05	0.13	0.002	0.35	0.06	0.05	0.10	0.01	50	.062	43.11
	Sample No.	SO3 %	Cl ppm	Ba ppm	Sr ppm	Cu ppm	Zn ppm	Pb ppm	Ni ppm	Cr ppm	V ppm	Ce ppm	La ppm
	1	0.128	1162	3	246	6	21	8	31	9	7	1	62
	2	0.183	435	6	223	3	117	1	27	4	10	41	50
	3	0.528	398	9	254	3	21	7	32	7	11	3	1
	4	0.135	399	8	206	6	22	1	32	7	9	2	1

Table 3. XRF results for the CaCO3 powder samples.

Sample No.	W Ppm	Mo ppm	Ga ppm	Nb ppm	Zr ppm	Y ppm	Rb ppm	Co ppm	As ppm	U ppm	Th ppm
1	1	1	4	5	43	2	12	4	10	1	3
2	1	2	2	13	37	1	15	1	23	1	9
3	1	1	4	2	44	2	13	6	34	1	2
4	1	1	5	5	39	2	18	11	23	1	6

Table 3. XRF results for the CaCO3 powder samples (Continued).



Sampling Mode Signal Accumulation Count :

: 1.60-0.10i Refractive Index Interval (sec) : _ Signal Averaging Count: 64

1 Max of Absorbance Range : 0.200

Min of Absorbance Range : 0.010

Ultrasonic Dispension Time (sec) :

Waiting Time After Ultrasonic Dispersion(sec) :

Figure 1. Distribution of the particle sizes based on the numbers of particles

Journal of Applied Geology, Summer 2013, Vol. 9, No. 2 w.SID.ir

SHIMADZU SALD-2101 (SALD-							LD-	2101	-WEA1:	V1.20)		
(File	Name) sam	ple 3										
(Samp	le ID)					(Sample #)					
(Da	tee)06/	02/15				(Time) 2	1:59:41	1			
R Ind	ex=1.60-0.	10i	Median D :	0.634		Mean V:	0.761		10.0%D:	0.430	SI	evel:0
			Modal D:	0.562		Std Dev :	0.278		50.0%D:	0.634	DF	unc: None
									90.0%D:	1.747	DS	hift :0
4	د											
1	50											
r r	ς 											
5	U -											
	- - -											
1	- 30											
É	ů.				28							
7	່ <u>2</u> 0				Ĭ -\-							
t -7	A -				/ ଧ୍							
	- 10				6							
						ઠ્						
						aaaa						
	0			2-0-0-		1			-0-0-0-0-		<u></u>	
	-					Parcicle D			(μ το			
	Diam	Cum	Diff		Diam	Cum	Dif	f		Diam	Cum	Diff
	ж(µm)	Q 1(%)	g ₁ (%)		х(µ т) Q ₁ (\$) q ₁	(%)		х(µm)	۹ <mark>۱</mark> (%)	9 ₁ (%)
1	1000.000	100.000	0.000	18	28.98	8 99.	390 C	.063	35	0.840	72.708	15.309
2	811.975	100.000	0.000	19	23.53	8 99.	327 0	.090	36	0.682	57.399	23.361
3	659.303	100.000	0.000	20	19.11	2 99.	737 0	.120	37	0.554	34.038	21.930
4	535.337	100.000	0.000	21	15.51	8 99.	517 0	.147	38	0.450	12.108	10.899
5	434.680	100.000	0.000	22	12.60	1 99.	170 0	.191	39	0.365	1.209	1,209
6	352.949	100.000	0.000	23	10.23	1 99.	279 0	.293	40	0.297	0.000	0.000
7	286.586	100.000	0.000	24	8.30	8 98.	986 0	.419	41	0.241	0.000	0.000
8	232.700	100.000	0.000	25	6.74	6 98.	567 0	.549	42	0.196	0.000	0.000
9	188.947	100.000	0.000	26	5.47	7 98.	J17 0	.726	43	0.159	0.000	0.000
10	153.420	100.000	0.000	27	4.44	/ 97.	292 0	.972	44	0.129	0.000	0.000
12	101 150	T00*000	0.001	28	3.61	1 96. D 05.	1 ورد 1		45	0.105	0.000	0.000
	101.120	33.333	0.003	29	2.93	د 2 کلا 1 02	/125 1	050	40	0.065	0.000	0.000
14	66 <u>6</u> 90	90 000	0.006	3U 21	2.38	- 55 בי יים ג	±JD 2 366 0	-009 0770	4/	0.009	0.000	0.000
15	54 149	99.990	0.012	32	1 57	0 85	500 Z		40	0.036	0.000	0.000
16	43 969	99 961	0.028	22	1 27	5 94		. 603	50	0.037	0.000	0.000
17	35,701	99,932	0.042	34	1.03	5 80.1	286 7	.578	51	0.030	0.000	0.000
Sampl	ing Mode	: 1	fanual Ref	iractive	Index	: 1	.60-0.10i					
Signa	l Accumula	tion Count :	1 Int	erval	(sec):_	Signal	. Averaging	Count	: 64			
Max o	f Absorban	ce Range : (0.200 Mir	n of Aba	arbance i	Range :(.010					
ultra	sonic Disp	ersion Time (s	sec): Wai	ting T	ine After	Ultrasonio	Dispension	n(sec)	:			

Figure 2. Distribution of the particles size based on longitude equivalent diameter

Esmaili Mahani & Azadi: Improve of Rubber Physical Properties with Addition of Waste Calcium Carbonate



Figure 3. Distribution of the particles size based on surface area equivalent diameter

The results from characterization of the four waste CaCO3 powder samples are summarized in Table 4. The mean numbers of particle size (selected sample) was 0.597μ m, the mean longitudinal equivalent

diameter was 0.761μ m, and mean surface area equivalent diameter was 0.974μ m. When sieved through a 325 mesh sieve (45 μ m), the average percentage of the CaCO3 that remained on the sieve

Journal of Applied Geology, Summer 2013, Vol. 9, No. 2, 173

was 0.356 %. The average purity of the powders was 98.50 %, and they were all white. These results

indicate the powders are suitable for use as fillers in production of rubbers and other rubber parts.

	Table 4. Characterization of the CaCO3 powders.										
Sample	Mean	Mean longitudinal diameter of particles	Mean specific area	Percentage	$CacO_3$	MgO	Fe_2O_3				
No.	particles	ulumeter of purifiers	diameter of	mesh sieve	MgcO ₃		Al_2O_3				
	μm	μm	μm	(43 μm) %	%	%	%				
l (selected sample)	0.597	0.761	0.974	0.356	97.259	0.34	0.11				
2	0.585	0.609	1.815	0.471	98.950	0.33	0.16				
3	0.558	0.616	1.651	0.411	98.619	0.39	0.22				
4	0.581	0.682	1.730	0.839	99.03	0.35	0.19				
·	-										

3.3. Testing of the tire product (Mechanical Properties)

The tensile properties were determined using an Instron universal testing machine (model Shimadzu xlv12, Shimadzu Co. Ltd., Kyoto, Japan) with a crosshead speed of 350 mm/min., and 1-kN load cell. The specimens were stamp-cut from a 2-mm-thick compression-moulded sheet (ASTM D412-92). 300% modulus (ASTM D412) and elongation at rupture (ASTM D1456) was also determined.

The sample hardness was determined using a shore A durometer (model DIA 7021, Shindong Co. Ltd., Japan) in accordance with ASTM D2240. It was determined at three different positions on the specimens (about 6-mm thick) and the median value was indicated. Each mechanical property test was repeated five times and an average value was used in the data analysis. Physical testing procedures were suitably followed the standard test methods which can be ASTM shown in table 5.

Table 5. Physical and mechanical testing of fourrubber samples produced with the waste CaCO3powders

Sample No.	Hardness	Tensile strength Kg/Cm ² (MPa)	Elongation at rupture %	300 % modulus Kg/Cm ² (MPa)
1	43	230(23)	588	70(7)
2	42	227(22.7)	582	71(7.1)
3	41	216(21.6)	583	69(6.9)
4	45	222(22.2)	590	70(7)
	40±5	150-300	350	> 40
Standard	ASTM D-2240	ASTM D-412	ASTM D-1456	ASTM D-412

4. Conclusions

Waste calcium carbonate from marble sawing was analyzed by XRF and DLS. The results showed it was similar to the fillers currently used in the rubber industry. Tires produced with this waste powder had similar properties to those produced with the standard filler. Therefore, the waste powder could be used as an inexpensive replacement filler.

Acknowledgment

The authors would like to thank islamic azad university of Neyriz branch, Neyriz, Iran. This article was taken from research project with support of islamic azad university of Neyriz Branch. Too, the authors would like to thank Miss Eng. P.Moshksar.

References

Ai-lon, W., Ting-xian, W., Feng-wei, Y., Qun-xu, H. & Peng-xiang, Y., 2012, "Rubber industry", *Published on Rubber Industry of China, Vol.* 48(9):11-27.

Bagghi, A.K. & Sharma, B.G., 1981, "Reinforcement and physical properties of filled rubber system", *Indian J. Technol., Vol. 19: 368-372.*

Boynton, R. S., 1980, "Chemistry and Technology of lime and limestone", *John Wiley, New York, 277 pp.*

Gent, A.N., 2001, "Engineering with rubber, How to design rubber components", 2nd Edition, Polymer Science 3909, The University of Akron, Akron OH 44325-0309, USA, 310 pp.

HsanZadeh, E., 2007, "The application of nano technology in rubber industry", *http://www.irche.com/Tires_and_Nano. aspx, Available in 16 July 2007.*

Katz, H. S., 1987, "Solid spherical fillers", *In: Katz, H. S., Milewski, J. V. (eds.), Handbook of fillers for plastics, Van Nostrand, New York, 429 pp.*

Kauffman, S. H., Leidner, J., Woodhams, R. T. & Xanthos, M., 1974, "The preparation and classification of high aspect ratio mica flakes for use in polymer reinforcement", *Powder Technology*, Vol. 9 (2-3):125-133 Lefond, S. J., 1983, "Industrial minerals and rocks", 5rd ed., Society of Mining Engineers, New York, 1478 pp. Poompradub, S., Luthikaviboon, T., Linpoo, S., Rojanathanes, R. & Prasassarakich, P., 2010, "Improving oxidan stability and mechanical properties of natural rubber vulcanizates filled with calcium carbonate modified by gallic acid", Polymer Bulletin, Vol. 65, Published online: 02 November 2010.

Richard, J. & Lewis, Sr., 2004, "Sax's Dangerous properties of industrial materials", 11 rd ed, Vol. 1-3, John Wiley & Sons, Inc, New York, 125 pp.

Strutz, M.D. & Sweeney, C.T., 1990, "Natural ground calcium carbonate", *Proceeding Tappi Neutral/Alkaline Short Course October, Tappi Press, Atlanta, Ga.: 16-18.*

Von Flotow, A.H. & Etkin, B., 1981, "Performance of the university of Toronto infrasizer MK III as a monosizer and multi-cut classifier", *Powder Technology, Elsevier, Vol. 30*(2):257-264.

Supporting Information

Filler	Mean particle size μm	Distribution of particles size µm	Particle shape	Specific gravity g/cm ³	Specific surface area (BET) m ² /g	Humidity %	CacO ₃	MgO %	Fe ₂ O ₃ + Al ₂ O ₃ %
Natural CaCO ₃	3-120	0.1-600	Cubic	2.7	0.3-2	≤0.5	≥94.5	≤ 0.7	\leq 0.3
Precipitated CaCO ₃	0.07-1	0.1-2	Cubic spherical	2.6	11-26	≤0.5	≥94.5	≤0.7	\leq 0.3

Table S1. Specifications for micronized calcium carbonate used in the rubber industry

 Table S2. Specifications for nanosize calcium carbonate used in the rubber industry (NPCC-GBT/9590-2004/Chinese Standard)

Filler	Mean particle size µm	Specific surface area (BET) m ² /g	Particle shape	Specific gravity g/cm ³	Filler brightness %	Humidity %	Color of CacO ₃	CacO ₃ %	MgO %	Al ₂ O ₃ + Fe ₂ O ₃ %
CaCO ₃	15-40	40	Cubic	2.7	≥ 88	≤ 0.5	White powder	\geq 94.5	≤ 0.7	\leq 0.3