



Development a Predictive Finite Element Model for Investigation of Phases Behavior after Cold Rolling Process

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ABSTRACT

One of the surface defects that arise in sheet metal working is when the part is removed from the die. Since there are no external forces to make this defect, the origin of such fail is known as residual stress. Residual stress can develop in sheet metal forming due to non-uniform deformation. In this paper, the workpiece is carbon steel with different volume fractions and arrangements of ferrite and pearlite. Due to different stress-strain curves for each phase after cold rolling, one phase deforms elastically, whereas the other undergoes elastic-plastic deformation. On unloading to zero applied stress, this effect can produce residual stress. Therefore, in order to reduce the surface defects in sheet metal forming, an intelligent predictive code using a validated elastic-plastic finite element method is generated for a plain strain deformation of cold rolling process. Results show that in regular arrangement of ferrite and pearlite, workpiece microstructure has great influence on the residual stress distribution, and by decreasing the width of each strip, the fluctuation of residual stress is reduced. The purpose of this study is to develop the state of the art instructions for arrangement of phases after hot rolling process where the total residual stress produced after cold rolling and sheet metal working will be minimized.

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1. INTRODUCTION

Metal forming is one of the production processes that is divided in two general categories of bulk and sheet forming. Rolling is one of the most important bulk forming processes in which the raw material is deformed by passing through minimum two rolls.

The main purpose of Rolling is reduction in the thickness of workpiece and it might be done both cold and hot. Process selection is dependent on type, size, materials, properties and final shape of the product. One of the consequences of cold rolling is work hardening of the metal that usually does not occur in hot rolling because of high temperature in rolling.

Throughout this century the rolling process has been analyzed by various analytical and numerical methods such as slab, the slip line, the upper bound and the finite element methods.

Among these, finite element method is one of the most commonly used methods used for analysis of rolling process. Until now, much work has been carried out on simulation of cold rolling with finite element method such as elastic-plastic finite element modelling of cold rolling of copper strip introduced by Liu et al. [1]. It shows that maximum pressure associated with the neutral point. In addition, the stresses and deformation of elements are presented.

Jiang and Tieu [2] have simulated three dimensional rigid plastic cold metal rolling. Later on they have simulated cold rolling process for ultrathin strips [3]. Zhang et al. [4] developed a fast rigid plastic finite element method for application in strip rolling. In order to improve computational efficiency and convergence Mej et al. [5] have proposed NR-BFGS method for fast rigid plastic FEM in strip rolling.

All the above-mentioned analyses were carried out with the assumption that the microstructure of the work materials was homogenous. In addition, Utsunomiya et al. [6] modelled rolling on the heterogeneous materials.

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They investigated roughening of matt surface in aluminium pack rolling experimentally and modelled that with finite element method [7].

In this paper, a finite element modelling of cold rolling has been developed for two phase alloy including ferrite and pearlite. It should be noted that almost all the metal to be rolled have multiple alloy phases and would deform heterogeneously. In this case a stress-strain relation of each element in workpiece is different according to type of the phase.

The novelty of this work is a discussion on the effect of the microstructure of the material and their arrangement on residual stress distribution. Residual stress has a great influence on surface quality of sheet metal. Developing a finite element code for calculation of residual stress in two phase alloys (ferrite and pearlite) can help engineers to propose the best structural arrangement of the phases which cause lower residual stresses and distortion, especially in pieces that are used in important mechanisms.

2. THE FINITE ELEMENT METHOD

2. 1. Modelling Assumption Figure 1 shows the geometry and the direction of the rolling process. In this simulation roller material is assumed rigid and the behaviour of the workpiece is elastic-plastic. Flat rolling of plates and sheets is essentially a plain strain compression because the length of contact between rollers and workpiece usually is much smaller than the width of the sheet.

The workpiece to be rolled is pure iron and three kinds of plain carbon steel having different arrangements and combination of ferrite and pearlite. In this states, sheet is formed from two phases. Figure 2 shows stress-strain curves of ferrite and pearlite.

According to Figure 2, stress-strain relation in plastic region is written as follows for ferrite:

$$\sigma_f = 620 (\varepsilon_p + 0.023)^{0.2} \quad (1)$$

And for pearlite:

$$\sigma_p = 1100 (\varepsilon_p + 0.0327)^{0.2} \quad (2)$$

2. 2. Friction Modelling Friction is an inseparable part of the rolling process. Unlike the others metal forming processes in which one tries to remove the friction, in rolling friction must be present as it controls the process.

It can be shown experimentally that material velocity at entry is slower than roll surface velocity, and faster at exit, so in the space between the two rolls, there is a section where the material velocity is equal to roll surface velocity: this point is called neutral point. Variation of material velocity relative to roll surface in

neutral point will result in varying local friction stress both in direction and magnitude. Therefore, neutral point divides the roll space in two regions as shown in Figure 3.

1. Backward slip zone: the friction stress τ have a resisting direction the deceleration of material moment, or the same as the rolling velocity direction.
2. Forward slip zone: the friction stress τ have a resisting direction the acceleration of material moment, or opposite to the rolling velocity direction [8].

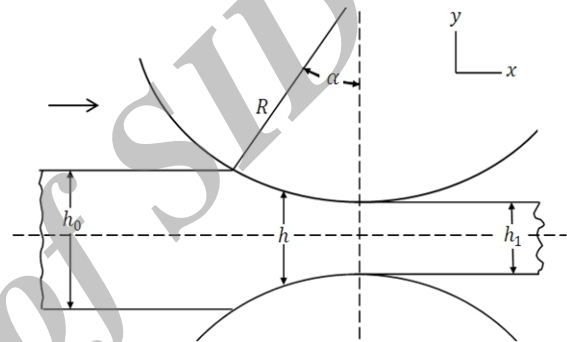


Figure 1. Geometry of rolling and its direction

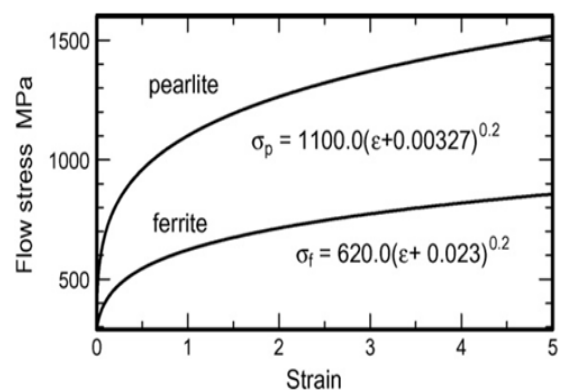


Figure 2. Stress-strain curve of ferrite and pearlite [9].

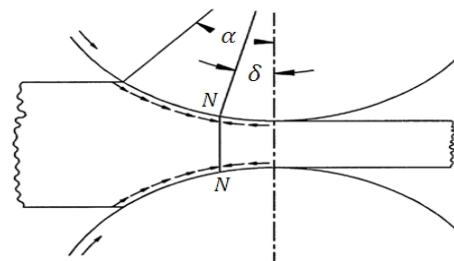


Figure 3. Neutral point and variation in friction stress direction

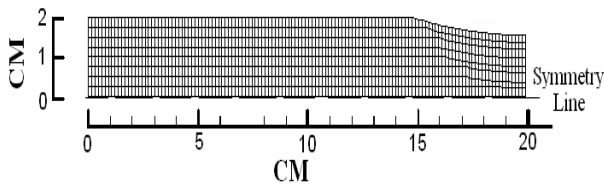


Figure 4. Primary meshing of workpiece include 1280 four nodes quadratic elements.

TABLE 1. Material's properties [10].

Young's modulus	Poisson's ratio
210 GPa	0.3

Considering the importance of friction in rolling process simulation, various theories are expressed for friction in flat rolling and researchers have studied various methods such as dynamic friction model, Amontons-coulomb and constant friction model for applying friction stress [11]. Distribution of contact stress for cold rolling in this paper is predicted by Amontons-coulomb friction model. In this model, friction stress τ is proportional to normal pressure (p):

$$\tau = \mu p \quad (3)$$

where μ is the coefficient of friction and in this research is considered 0.2.

2. 3. Finite Element Solution The finite element method is now firmly acceptable as a most powerful general technique for the numerical solution of a variety of problems encountered in engineering. The first step in solving finite element problems is meshing the workpiece in which the problem is divided into a number of small problems.

Figure 4 shows the primary meshing of workpiece. In rolling simulation, because of the deformation is symmetric about the midline between the rolls, only half of the piece is considered.

Due to the symmetry of about the midline between rolls, only half of the workpiece is modelled. Frictional force acting between the roll and the workpiece draws the workpiece into the roll gap and causes movement of the workpiece.

In this paper, the rolling process has been simulated using an elastic-plastic finite element method for plain strain deformation for isotropic work hardening, which includes both material and geometric nonlinearity. It permits the identification of elastic and plastic deformation in rolling and also the effect of unloading.

An elastic analysis is carried out to get the initial stress at first. The equivalent stress using the von Mises yield criterion is used to compare obtained stresses to

the yield stress. Then, in the next step if the equivalent stress in previous step was smaller than the yield stress, the problem is solved elastically again, but if it is larger, it means that the deformation has already entered the plastic region.

Hook's law for the isotropic elastic material is used. Based on the flow rules and normalized hypothesis equation on plastic region could be expressed [12]:

$$\{d\sigma\} = [D^{ep}] \{d\varepsilon\} \quad (4)$$

$$D^{ep} = D^e - \frac{dD^e \cdot dD^e}{H' + dD^e \cdot a}, dD^e = D^e a \quad (5)$$

$$H' = \frac{d\bar{\sigma}}{d\bar{\varepsilon}^p} \quad (6)$$

In the above equation H' is work-hardening. Work hardening in plastic zone which has strong influence on the results, is derived from Equations (1) and (2). D^e is the elastic stress-strain matrix which for the plain strain deformation is:

$$[D^e] = \frac{E}{(1+\nu)(1-2\nu)} \begin{bmatrix} 1-\nu & \nu & 0 \\ \nu & 1-\nu & 0 \\ 0 & 0 & \frac{1-2\nu}{2} \end{bmatrix} \quad (7)$$

E and ν are Young's modulus and Poisson's ratio, respectively which are shown in Table 1. a can be determined based on the yield criterion -here, the von Mises yield criterion, that is:

$$a = \frac{\sqrt{3}}{2 J_2^{1/2}} \{\sigma'_x, \sigma'_y, 2\tau_{xy}\} \quad (8)$$

In the above equation σ'_{ij} and J_2' are deviatoric stress and second invariant of deviatoric stress, respectively [11].

3. RESULT AND DISCUSSION

3. 1. Stress Distribution In this paper, stress distribution and their values as shown as Figure 5, has been calculated for pure iron in cold rolling process and plain strain state, using finite element formulation. The accuracy of these results has been proven with a commercial software as shown in Figure 6 [9, 13].

As mentioned, in this work, the unloading effect is considered. To prove that, stress behaviour on one element exiting from the gap between the rolls is shown in Figure 7.

3. 2. Residual Stress for Different Microstructures Residual stress for pure iron and some different carbon steels are discussed The results in this section are calculated for each vertical column passing from the

rollers region with averaging of stresses value for a column.

In continuation of this paper microstructures of elements are illustrated. Finite elements of ferrite and pearlite are also shown in black and white, but the deformation of elements is neglected. Average residual stresses for arrangements of phases are shown in Figures 8 to 10. Figure 8 shows the value of residual equivalent stress for the pieces having all their elements in one phase. As shown in Figure 8, since all the elements are in one phase, residual stress value in both of them is converging to a certain amount corresponding to their phase. It is quite clear that the values of residual equivalent stress in pearlite elements are more than ferrite. Figure 9 shows the value of residual equivalent stress for the two type of arrangement with different strip widths.

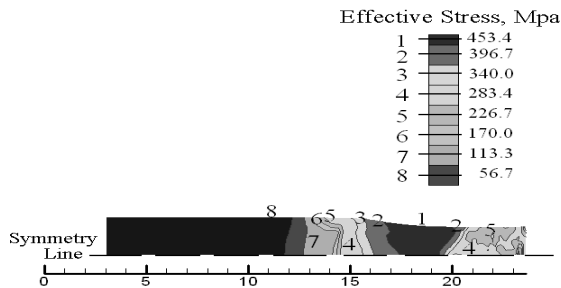


Figure 5. Effective Von Mises stress distribution for pure iron with FEM after 3 cm movement of sheet.

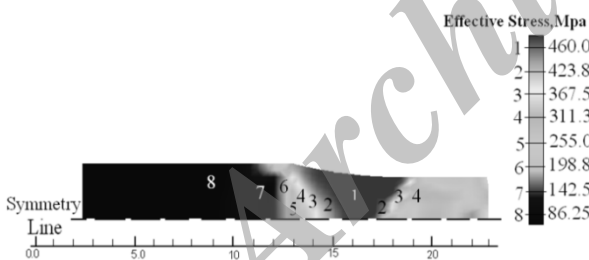


Figure 6. Effective Von Mises stress distribution for pure iron with Deform software after 3 cm movement of sheet.

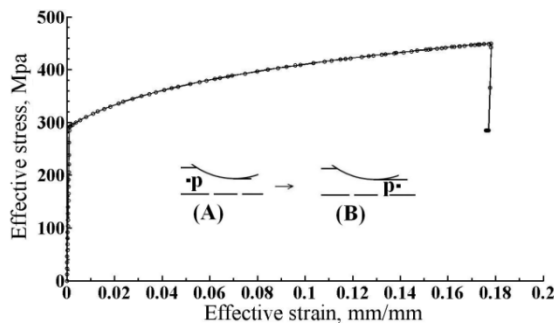
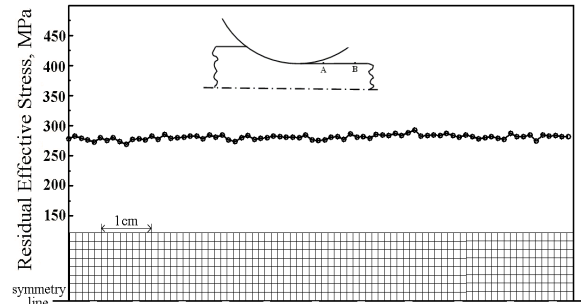
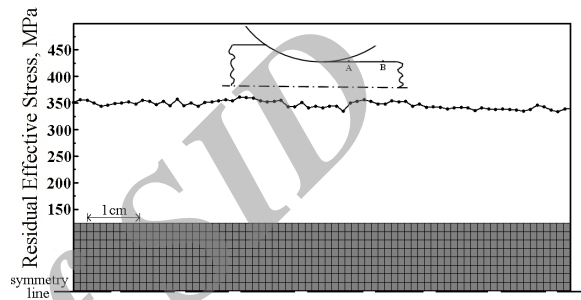


Figure 7. Stress-strain curve of shown element (p) during the movement from state1 to state 2.

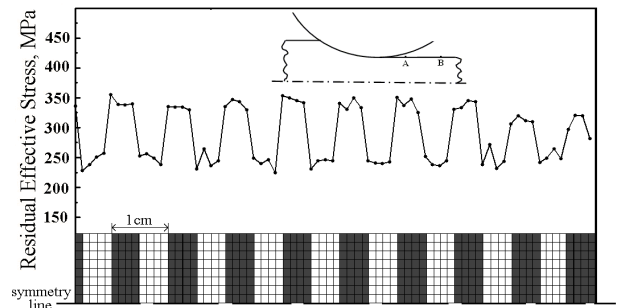


(a) For ferrite element.

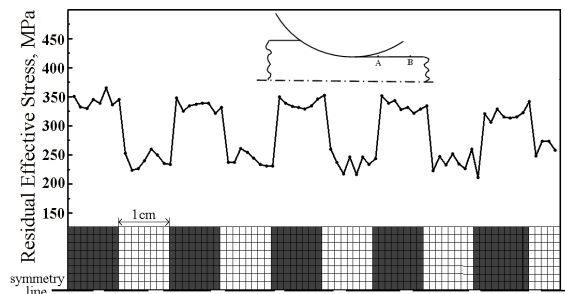


(b) For pearlite element

Figure 8. Residual stress in a column of elements that exit from roller's gap (from A to B).



(a) For narrow strips of elements.



(b) For narrow strips of elements.

Figure 9. Residual stress in a column of element in two phase arrangements with ferrite (white) and pearlite (black) (from A to B) in a vertical column.

As shown in Figure 9, residual equivalent stress values in both of them have fluctuations because of difference in flow stresses of ferrite and pearlite.

For two types of arrangements with different widths of strips it can be said that maximum value of residual stress is related to pearlite elements and minimum is for ferrite.

In Figure 9, maximum value of residual stress in broad stripes is larger than that of narrow ones. The opposite is true for the minimum value of residual stress. Hence, the fluctuation of residual stress would be reduced by decreasing the width of stripes of pearlite and ferrite, because by increasing the widths of stripes of pearlite and ferrite peaks and valleys values of residual stresses become larger and smaller respectively.

The phases arranged with the fluctuation of residual stress a column. Two models are chosen. In the first model the middle rows are pearlite and the rows on both sides are ferrite, and the second model is the opposite.. In this work, only half of the workpiece along y is considered, hence, the arrangements of phases are as shown in Figure 10.

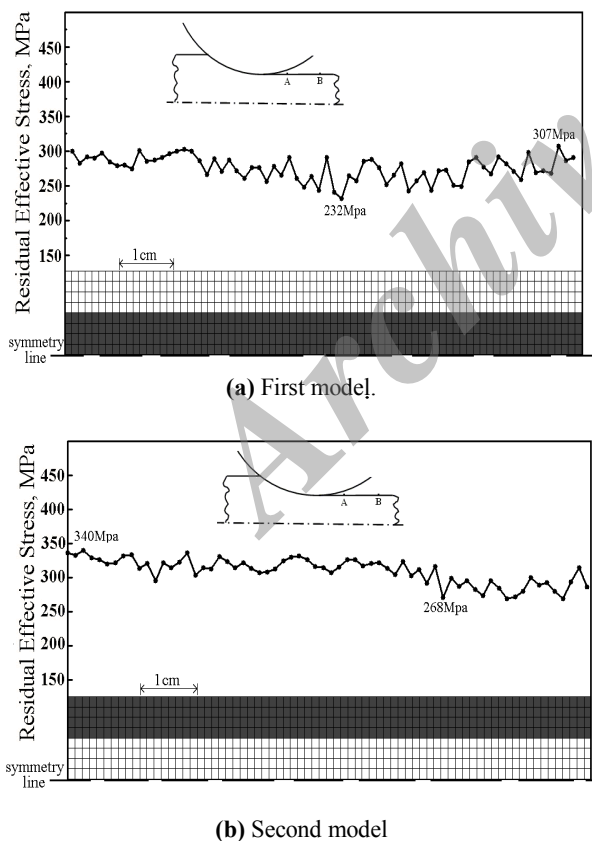


Figure 10. Residual stress in a column of element in two phase arrangements with ferrite (white) and pearlite (black) (from A to B) in horizontal row.

In these models, fluctuation in residual stress is less than that of the models in Figure 9. Comparing Figures 9 and 10 shows that variation in residual stress in the first model is more than that of the second one.

4. CONCLUSION

Microstructures of workpiece have a great influence on magnitude of residual stress on final sheet and the residual stress on pearlite elements are more than ferrite. Therefore, in rolling process, microstructure does not dissemble for evaluating residual stress. In regular arrangement of phases in sheet, by decreasing the width of stripes, the fluctuation of residual stress will be reduced.

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اغلب عیوب سطحی در فرایندهای شکل‌دهی فلزات بعد از خروج قطعه از قالب به وجود می‌آید. از آن جای که در این مرحله هیچ نیروی خارجی به قطعه اعمال نمی‌شود، بنابراین آنچه باعث بوجود آمدن این عیوب می‌شود تنش‌های پسماند است. تنش‌های پسماند در فرایندهای شکل‌دهی باعث تغییر شکل‌های غیریکنواخت می‌شود. در این مقاله قطعه‌کار از جنس فولاد دوفازی با کسر حجمی و آرایش‌های مختلف از فریت و پرلیت در نظر گرفته شده است که در آن به دلیل تفاوت رفتار تنش-کرنش فازهای مختلف بعد از نورد سرد، در حالی که یک فاز هنوز در ناحیه الاستیک قرار دارد فاز دیگر دچار تغییر شکل پلاستیک شده است و در هنگام باربرداری از قطعه این اثرات می‌تواند سبب به وجود آوردن تنش‌های پسماند شوند. بنابراین، برای کاهش این عیوب در ورق‌های ناشی از فرایندهای شکل‌دهی با استفاده از برنامه‌ی المان محدودی که صحت آن در ناحیه الاستیک-پلاستیک به تایید رسیده است به مدلسازی فرایند نورد سرد در حالت کرنش صفحه‌ای پرداخته می‌شود. نتایج به دست آمده نشان می‌دهد که در آرایش‌های منظم از فازهای فریت و پرلیت ساختارهای میکروسکوپی قطعه‌کار نقش مهمی را در پخش تنش پسماند داشته و با کاهش عرض این نوارهای فازی نوسانات در تنش‌های پسماند نیز کاهش می‌یابد. بنابراین هدف از این مطالعه ارائه ساختاری از چیدمان فازها بعد از نورد گرم است که در آن تنش پسماند نهایی قطعه کاهش یابد.

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