

()

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(// : // :)

K / K K BC₂ BC₁ F₂ F₁ Mo

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Zea mays L.

()

() .()

K
 (P_2) (P_1) K
 BC_2 BC_1 F_2 F_1
 K /
 F_2 F_1 (P_2) Mo (P_1)
 BC_2 BC_1

(RCBD)

F_1
 F_2
 BC_2 BC_1

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SAS

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-
1. Randomized Complete Block Design
 2. Duncan's Multiple Range Test

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(V_D) (V_A)

Excel 2000

(V_{AD})

$$\begin{aligned} V_A &= (2S_{F2}^2 - S^2 BC_1 - S^2 BC_2) \\ V_D &= (S^2 BC_1 + S^2 BC_2 - S_{F2}^2 - V_E) \end{aligned}$$

$$V_{AD} = \frac{1}{2}(S^2 BC_2 - S^2 BC_1)$$

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F_2 F_1 P_2 P_1

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BC_2 BC_1

$$V_E = \frac{1}{4}(S^2 P_1 + S^2 P_2 + 2S^2 F_1)$$

F_2

()

$$h_b^2 = \frac{V_{F2} - \sqrt{V_{P1} \times V_{P2}}}{V_{F2}}$$

(h)

(d)

l j i h d

(m)

()

$$h_b^2 = \frac{V_{F2} - \sqrt{V_{F1} \times V_{P1} \times V_{P2}}}{V_{F2}}$$

A

D C B

()

$$h_b^2 = \frac{V_{F2} - \frac{(V_{P1} + V_{P2} + V_{F1})}{3}}{V_{F2}}$$

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$$h_n^2 = \frac{2V_{F2} - (V_{Bc1} + V_{Bc2})}{V_{F2}}$$

%

F_1

1. Scaling tests
2. T-test

(d) (j) (j) K K

() P_2 P_1 F_2 F_2 K K

F_1 K / F_2 K / Mo

C B A () D

(l) K K

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$$\left(\frac{\sqrt{2V_D}}{V_A}\right)$$

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V_{AD}

K ×K

BC_2	BC_1	F_2	F_1	$P_2(K_{18})$	$P_1(K_{3218})$	
/ C	/ B	/ B	/ A	/ D	/ D	(Cm)
/ D	/ C	/ B	/ A	/ F	/ E	(Cm)
/ C	/ B	/ B	/ A	/ D	/ C	
/ B	/ A	/ AB	/ A	/ C	/ B	
/ AB	/ D	/ DC	/ A	/ BC	/ E	(Cm ²)
/ E	/ A	/ D	/ C	/	/ B	
/ DC	/ DE	/ C	/ A	/ B	/ E	(Cm)
/ B	/ C	/ B	/ A	/ BC	/ D	
/ B	/ C	/ BC	/ A	/ C	/ D	
/ C	/ D	/ B	/ A	/ B	/ C	(mgr)
/ BC	/ D	/ B	/ A	/ C	/ D	(gr)
/ C	/ C	/ B	/ B	/ C	/ A	(Cm)
/ C	/ B	/ C	/ C	/ C	/ A	
/ BC	/ D	/ BC	/ A	/ B	/ E	(Cm)
/ B	/ C	/ B	/ A	/ B	/ D	(gr)
/ B	/ B	/ B	/ C	/ AB	/ A	(Cm)
/ D	/ C	/ AB	/ BC	/ BC	/ A	(Cm)

%

Mo × K /

F_1						
/ B	/ D	/ C	/ A	/ D	/ E	(Cm)
/ B	/ C	/ B	/ A	/ C	/ D	(Cm)
/ B	/ B	/ B	/ A	/ C	/ C	
/ C	/ A	/ B	/ AB	/ C	/ A	
/ B	/ BC	/ BCD	/ A	/ DC	/ D	(Cm ²)
/ AB	/ A	/ B	/ AB	/ C	/ C	
/ B	/ D	/ CD	/ B	/ A	/ D	(Cm)
/ A	/ C	/ B	/ A	/ AB	/ C	
/ C	/ B	/ B	/ B	/ D	/ A	
/ B	/ C	/ B	/ A	/ A	/ C	(mgr)
/ B	/ D	/ C	/ A	/ D	/ C	(gr)
/ BC	/ B	/ B	/ B	/ C	/ A	(Cm)
/ B	/ A	/ B	/ B	/ C	/ A	
/ B	/ B	/ B	/ A	/ B	/ B	(Cm)
/ B	/ D	/ B	/ A	/ C	/ C	(gr)
/ B	/ A	/ A	/ B	/ A	/ B	(Cm)
/ AB	/ C	/ BC	/ C	/ A	/ D	(Cm)

%

K × K

X^2	l	j	i	h	d	m
/ ns		/ *± /	/ *± /	/ **± /	/ ns ± /	/ ** ± /
/ ns	/ **± /	/ *± /	/ **± /	/ **± /	/ ** ± /	/ **± /
/ ns	/ **± /	/ **± /		/ ** ± /	/ *± /	/ **± /
/ ns			/ + ± /	/ **± /	/ **± /	/ **± /
/ ns	/ * ± /			/ **± /	/ **± /	/ **± /
/ +	/ **± /		/ **± /	/ **± /	/ **± /	/ ** ± /
/ *	/ **± /			/ + ± /	/ **± /	/ **± /
/ ns	/ **± /	/ **± /		/ * ± /	/ **± /	/ **± /
/ ns	/ **± /	/ + ± /	/ **± /	/ **± /	/ + ± /	/ **± /
/ ns	/ **± /	/ + ± /	/ **± /	/ **± /	/ **± /	/ **± /
/ ns	/ **± /	/ + ± /	/ **± /	/ **± /	/ **± /	/ ** ± /
/ ns				/ **± /	/ **± /	/ **± /
/ ns				/ **± /	/ **± /	/ **± /
/ ns	/ **± /	/ + ± /	/ **± /	/ **± /	/ ** ± /	/ **± /
/ ns				/ **± /	/ ns ± /	/ **± /
/ ns	/ **± /		/ **± /	/ **± /	/ ** ± /	/ **± /

** * + ns

K / × MO

X^2	l	j	i	h	d	m
ns	**	**		**	**	**
/	/ ± /	/ ± /		/ ± /	/ ± /	/ ± /
ns	**	*	*	+	**	**
/	/ ± /	/ ± /	/ ± /	/ ± /	/ ± /	/ ± /
ns			**	**	*	**
/			/ ± /	/ ± /	/ ± /	/ ± /
ns	**			**	+	**
/	/ ± /			/ ± /	/ ± /	/ ± /
ns			**	**	**	**
/			/ ± /	/ ± /	/ ± /	/ ± /
ns		*	**	**	**	**
/		/ ± /	/ ± /	/ ± /	/ ± /	/ ± /
*	**	**		*	**	**
/	/ ± /	/ ± /		/ ± /	/ ± /	/ ± /
ns	**	**		+	**	**
/	/ ± /	/ ± /		/ ± /	/ ± /	/ ± /
ns	**	**		+	*	**
/	/ ± /	/ ± /		/ ± /	/ ± /	/ ± /
ns	**	**	**	**	**	**
/	/ ± /	/ ± /	/ ± /	/ ± /	/ ± /	/ ± /
ns			*	*	**	**
/			/ ± /	/ ± /	/ ± /	/ ± /
ns	**	**		+	+	**
/	/ ± /	/ ± /		/ ± /	/ ± /	/ ± /
ns	**	**		**	ns	**
/	/ ± /	/ ± /		/ ± /	/ ± /	/ ± /
*		**		**	**	**
/		/ ± /		/ ± /	/ ± /	/ ± /
ns		*	ns	+	**	**
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** * + ns

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