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**(Visual Basic )**

**( DAFI )**

**Determination of Areas Flooding Intensity )**

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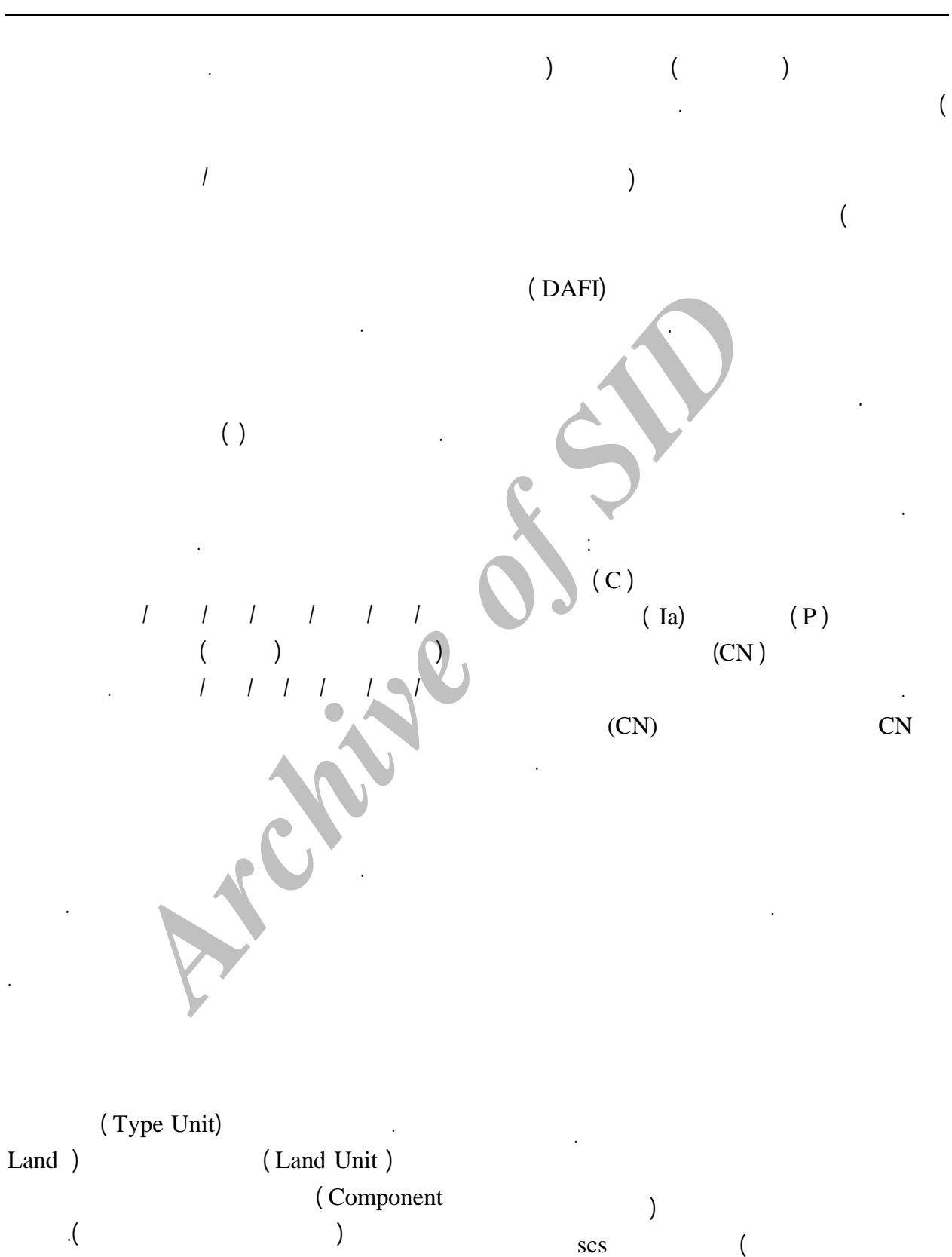
) SCS

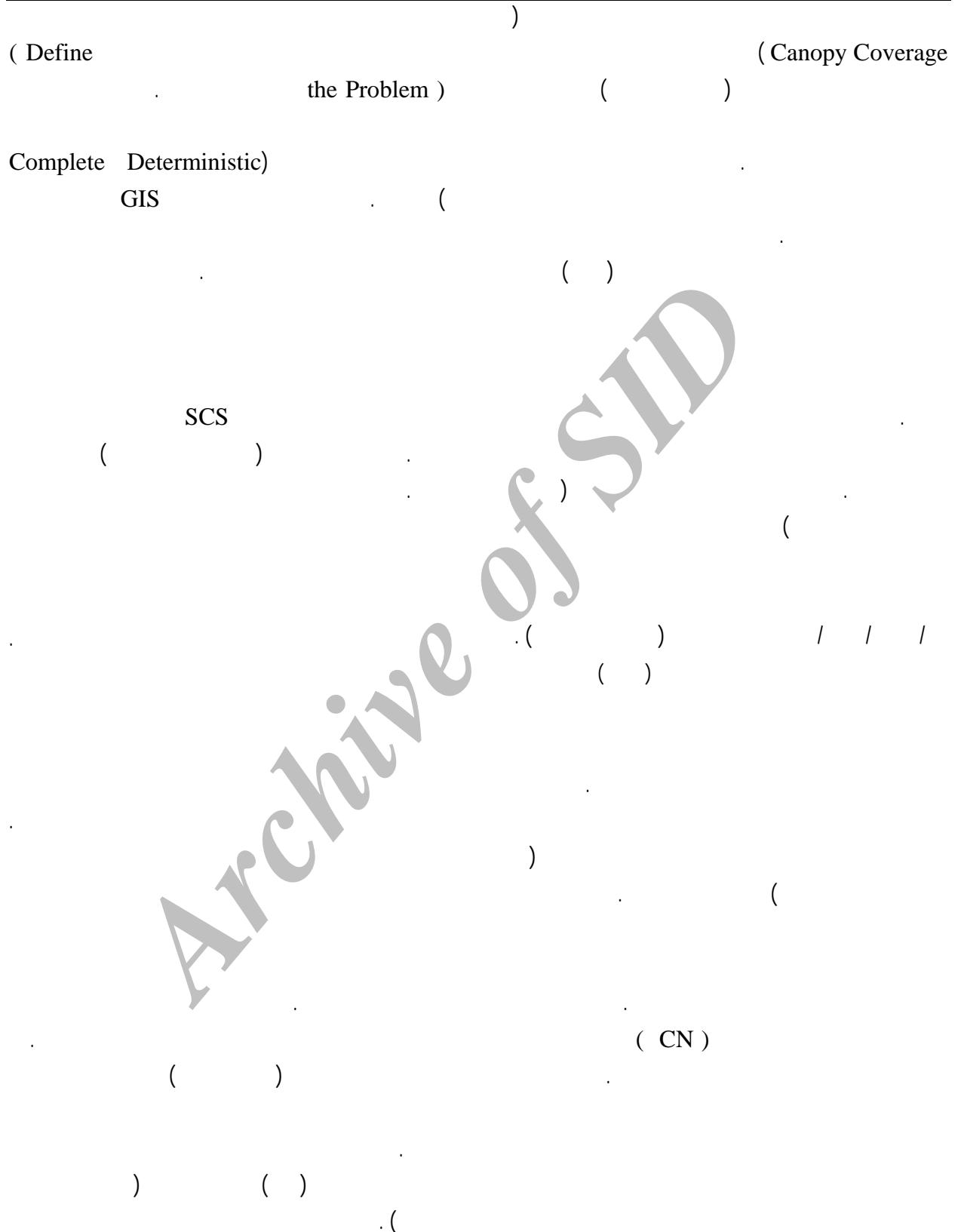
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Curve )  
CN              ( Least Squares )              (Fitting

W  
WL              D  
City

(A,B,C,D)

Type Unit  
( Land Unit )

$C$

$P_o \leq P \langle P_s \rangle$

$C = \frac{\left[ 1 - \frac{\lambda}{P} \left( \frac{1000}{CN} - 10 \right)^2 \right]}{1 + \frac{(1-\lambda)}{P} \left( \frac{1000}{CN} - 100 \right)}$

$C = 1 - \frac{1}{P} \left( \frac{1000}{CN} - 10 \right) \quad P \geq P_s$

Ia .              0.25               $\lambda$

Q               $S'$               (              )              Ia    P

M2-.    M1-2   )              D  
          . ( M1-3 . H1-1 . M2-3 . M2-2 . 1  
          . C1-1 )              C  
H2-3    H1-3    H1-2    H1-2    C1-3 . C1-2  
          . ( T1-2 . H2-2 . T2-2 . T2-1  
M1-3 . P2-2 )              B  
          . ( CF1-1 )              A  
          . (              )              ( X1-1

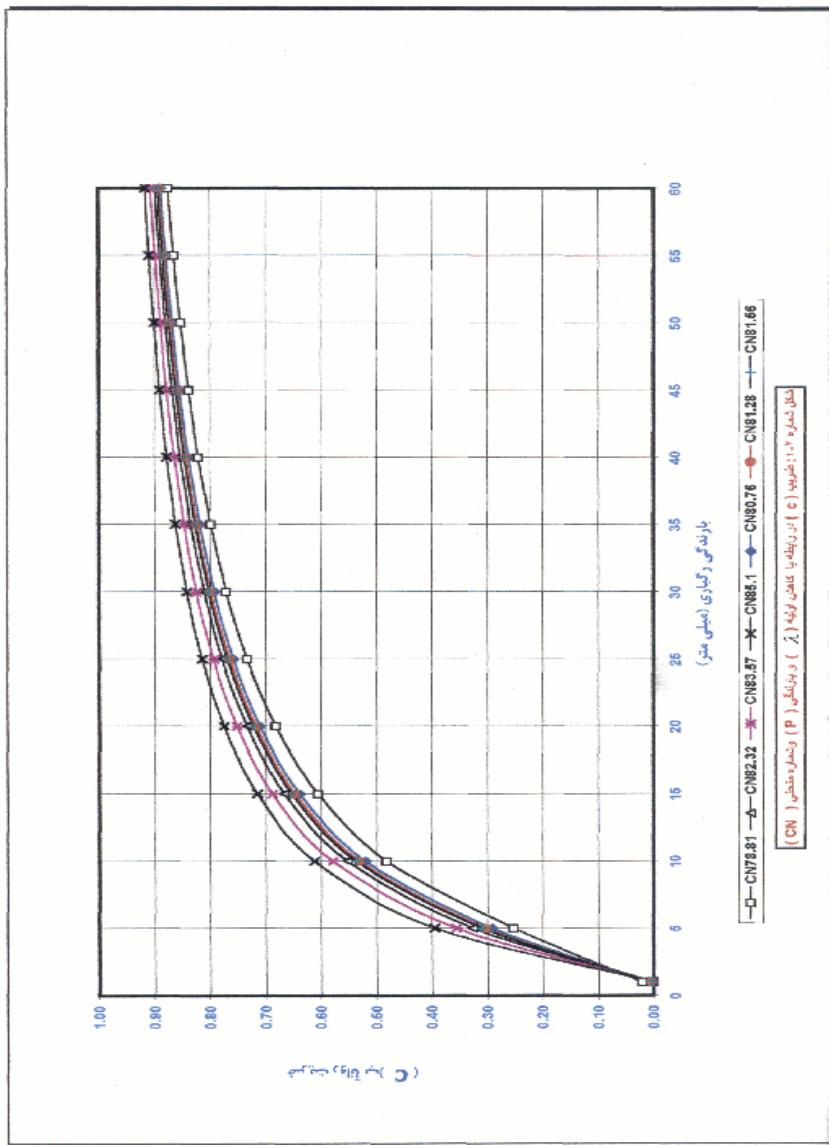
CN

$$\begin{array}{ccccccc}
 & CN & P & \lambda & & (C) \\
 C & & \frac{\partial c}{\partial CN} & \frac{\partial c}{\partial p} & \frac{\partial c}{\partial \lambda} & \\
 & & CN & P, & \lambda & \\
 dCN & dp & d\lambda & & & dc \\
 C & & & & & \\
 P & CN & & CN & P & \lambda & \lambda \\
 & & & & & & \\
 dc = & \frac{\partial c}{\partial \lambda} d\lambda + \frac{\partial c}{\partial p} dp + \frac{\partial c}{\partial CN} dCN & & & & & ( ) \\
 & & & & & & \\
 \frac{dc}{C} = & \left( \frac{\partial \lambda}{\partial \lambda} \frac{\lambda}{C} \right) \frac{\partial \lambda}{\lambda} + \left( \frac{\partial c}{\partial p} \frac{p}{c} \right) \frac{dp}{p} + \left( \frac{\partial c}{dCN} \frac{CN}{C} \right) \frac{dCN}{CN} & & & & & ( ) \\
 & & & & & & \\
 \frac{\partial c}{\partial \lambda} \frac{\lambda}{c} = & \frac{Po}{p} \left[ 1 + \frac{2(1-\lambda)}{\lambda} \frac{Po}{p} - \frac{2-\lambda}{\lambda} \left( \frac{Po}{P} \right)^2 \right] & & & & & ( ) \\
 & & \left( 1 - \frac{Po}{P} \right)^2 \left( 1 + \frac{1-\lambda}{\lambda} \frac{Po}{p} \right) & & & & \\
 & & & & & & \\
 \frac{\partial c}{\partial p} \frac{p}{c} = & \frac{1}{\lambda} \frac{Po}{P} \left[ 1 + \lambda + (1-\lambda) \frac{Po}{P} \right] & & & & & ( ) \\
 & & \left( 1 - \frac{Po}{P} \right) \left( 1 - \frac{1-\lambda}{\lambda} \frac{Po}{P} \right) & & & & \\
 & & & & & & \\
 \frac{\partial c}{\partial CN} \frac{CN}{c} = & \frac{\left( \frac{po}{\lambda} + 10 \right) \left[ \frac{1+\lambda}{p} + \frac{1-\lambda}{\lambda} \left( \frac{po}{p} \right)^2 \right]}{\left( 1 - \frac{Po}{P} \right) \left( 1 - \frac{1-\lambda}{\lambda} \frac{Po}{P} \right)} & & & & & ( )
 \end{array}$$

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جدول شماره ۲۳-۲۴ ضریب (C) در رابطه با کاهش اولیه (ج) واردگی (IP) و شماره مبتدا (CN)

	100	90	80	70	60	50	40	30	20	10	P
1	0.083	0.038	0.023	0.015	0.010	0.007	0.004	0.002	0.001	1	
1	0.474	0.286	0.189	0.130	0.091	0.063	0.041	0.024	0.011	3	
1	0.643	0.444	0.318	0.231	0.167	0.118	0.079	0.048	0.022	6	
1	0.730	0.646	0.412	0.310	0.231	0.167	0.114	0.070	0.032	9	
1	0.783	0.615	0.483	0.375	0.286	0.211	0.146	0.091	0.043	12	
1	0.818	0.667	0.638	0.429	0.333	0.250	0.176	0.111	0.053	16	
1	0.844	0.706	0.683	0.474	0.375	0.286	0.206	0.130	0.063	18	
1	0.863	0.737	0.620	0.512	0.412	0.318	0.231	0.149	0.072	21	
1	0.874	0.762	0.651	0.645	0.444	0.348	0.265	0.187	0.082	24	
1	0.890	0.783	0.677	0.574	0.474	0.375	0.278	0.184	0.091	27	
1	0.900	0.800	0.700	0.600	0.500	0.400	0.300	0.200	0.100	30	
1	0.908	0.815	0.720	0.623	0.524	0.423	0.320	0.216	0.109	33	
1	0.915	0.828	0.737	0.643	0.545	0.444	0.340	0.231	0.118	36	
1	0.921	0.839	0.752	0.661	0.565	0.464	0.360	0.245	0.126	39	
1	0.926	0.848	0.766	0.677	0.583	0.483	0.375	0.259	0.135	42	
1	0.931	0.857	0.778	0.692	0.600	0.500	0.391	0.273	0.143	45	
1	0.935	0.865	0.789	0.706	0.616	0.516	0.407	0.286	0.151	48	



جدول شماره ۱-۴: حساسیت ضریب روابط (C) به نسبت کاهش اولیه ( $\lambda$ )

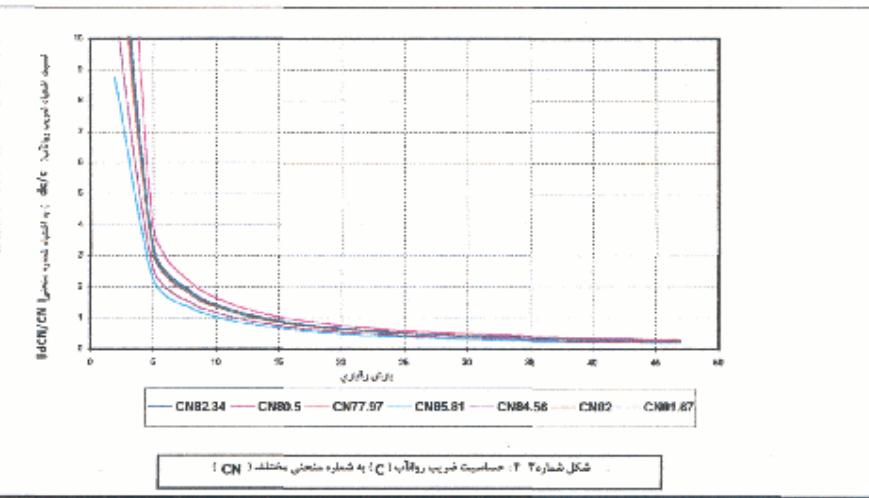
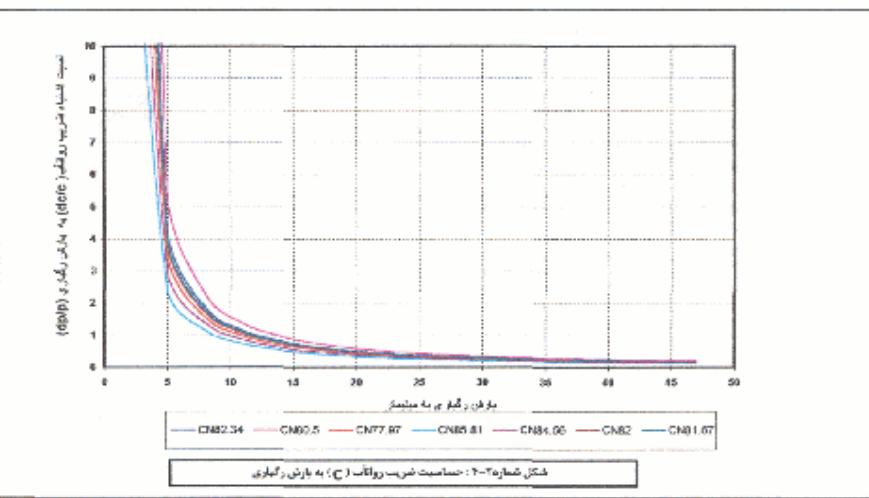
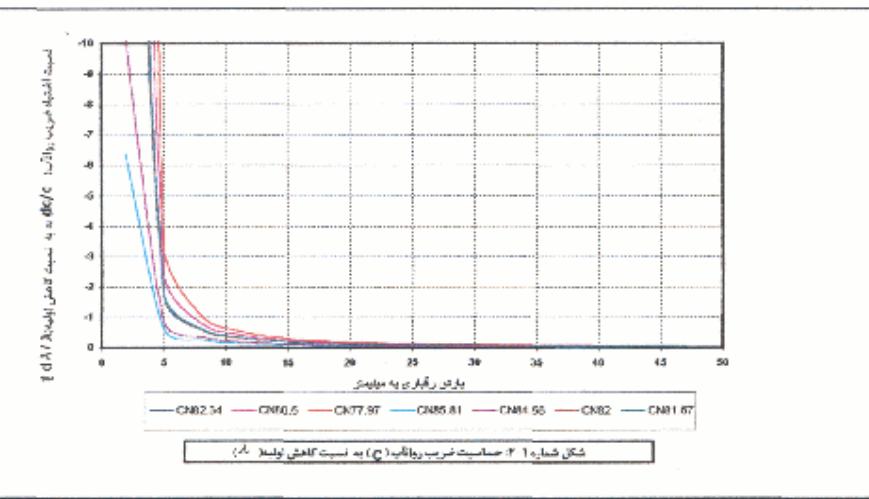
UNIT-1	UNIT-2	UNIT-3	UNIT-4	UNIT-5	UNIT-6	TOTAL	P
82.34	80.5	77.97	85.81	84.56	82	81.67	
-26.874	-49.514	-92.812	-6.349	-10.127	-28.007	-29.728	2
-1.73	-2.50	-3.49	-0.65	-0.90	-1.78	-1.85	5
-0.598	-0.819	-1.084	-0.257	-0.342	-0.612	-0.632	8
-0.317	-0.422	-0.543	-0.149	-0.191	-0.324	-0.333	11
-0.204	-0.266	-0.337	-0.1	-0.127	-0.208	-0.214	14
-0.147	-0.188	-0.238	-0.075	-0.094	-0.149	-0.163	17
-0.113	-0.143	-0.176	-0.059	-0.073	-0.115	-0.117	20
-0.091	-0.114	-0.14	-0.049	-0.06	-0.092	-0.094	23
-0.076	-0.094	-0.114	-0.041	-0.051	-0.077	-0.078	26
-0.064	-0.08	-0.098	-0.036	-0.044	-0.065	-0.067	29
-0.056	-0.069	-0.083	-0.031	-0.038	-0.057	-0.058	32
-0.049	-0.061	-0.073	-0.028	-0.034	-0.05	-0.051	35
-0.044	-0.054	-0.064	-0.025	-0.031	-0.045	-0.048	38
-0.04	-0.048	-0.058	-0.023	-0.028	-0.04	-0.041	41
-0.036	-0.044	-0.052	-0.021	-0.025	-0.037	-0.038	44
-0.033	-0.04	-0.048	-0.019	-0.023	-0.034	-0.034	47

جدول شماره ۲-۴: حساسیت ضریب روابط (C) به بارش و گباری (P)

UNIT-1	UNIT-2	UNIT-3	UNIT-4	UNIT-5	UNIT-6	TOTAL	P
82.34	80.5	77.97	UNIT-4	84.56	82	81.67	
44.137	70.188	31.251	17.313	23.912	36.901	39.266	2
4.38	5.579	3.583	2.485	3.053	3.953	4.102	5
1.89	2.316	1.598	1.165	1.39	1.735	1.788	8
1.147	1.379	0.984	0.736	0.866	1.061	1.09	11
0.808	0.96	0.7	0.532	0.621	0.751	0.771	14
0.619	0.73	0.539	0.415	0.481	0.577	0.591	17
0.499	0.685	0.437	0.339	0.391	0.467	0.478	20
0.418	0.487	0.367	0.286	0.329	0.391	0.4	23
0.358	0.417	0.316	0.247	0.284	0.336	0.344	26
0.313	0.364	0.277	0.217	0.249	0.294	0.301	29
0.278	0.322	0.248	0.194	0.222	0.262	0.267	32
0.25	0.289	0.222	0.175	0.2	0.236	0.24	35
0.227	0.262	0.202	0.16	0.182	0.214	0.218	38
0.208	0.24	0.185	0.147	0.167	0.196	0.2	41
0.192	0.221	0.17	0.136	0.154	0.181	0.185	44
0.178	0.204	0.158	0.126	0.143	0.168	0.171	47

جدول شماره ۲-۵: حساسیت ضریب روابط (C) به شماره منحنی مختلف (CN)

UNIT-1	UNIT-2	UNIT-3	UNIT-4	UNIT-5	UNIT-6	TOTAL	P
82.34	80.50	77.97	85.81	84.56	82.00	81.67	
15.975	23.885	14.317	8.741	10.892	14.761	15.431	2
3.343	3.974	3.226	2.301	2.643	3.157	3.233	5
1.858	2.155	1.810	1.322	1.502	1.760	1.788	8
1.285	1.477	1.258	0.927	1.043	1.219	1.244	11
0.923	1.124	0.963	0.713	0.806	0.932	0.951	14
0.785	0.906	0.781	0.680	0.663	0.766	0.770	17
0.668	0.760	0.656	0.489	0.549	0.634	0.646	20
0.578	0.654	0.566	0.422	0.474	0.547	0.557	23
0.506	0.574	0.497	0.371	0.417	0.480	0.490	26
0.451	0.511	0.444	0.332	0.372	0.428	0.437	29
0.407	0.461	0.401	0.300	0.336	0.387	0.394	32
0.371	0.420	0.365	0.273	0.306	0.352	0.358	35
0.341	0.385	0.335	0.251	0.281	0.323	0.330	38
0.315	0.356	0.310	0.232	0.260	0.299	0.305	41
0.293	0.331	0.288	0.216	0.242	0.278	0.283	44
0.274	0.309	0.269	0.202	0.226	0.260	0.265	47



( RR = Regcted Region )

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( ))

$$T = \frac{\overline{X - U_o}}{6/\sqrt{n}} = \frac{83.66 - 81.67}{2.902/11} = 2.274 \quad ( )$$

n = 12

2.274 T 2.902

$$\frac{\alpha}{z} \quad t$$

$$= 2.021 \frac{t\alpha}{2} \quad df = 11$$

( )

o:u =

/ (H uo)

CN

CN

/

(

Dimensionless Hydrograph )

/ CN

/

$$\frac{T}{Tp}$$

CN

)

Ho

Ha

$$\left( \frac{q}{qp} \right) A, \Delta D, tc, qp, tr, tb, tp ($$

( ) (u)

( uo)

( qp=33 D= 1.5 Tp= 7.5 Tc= 12.4)

( CN=81.67)

H o : u = uo

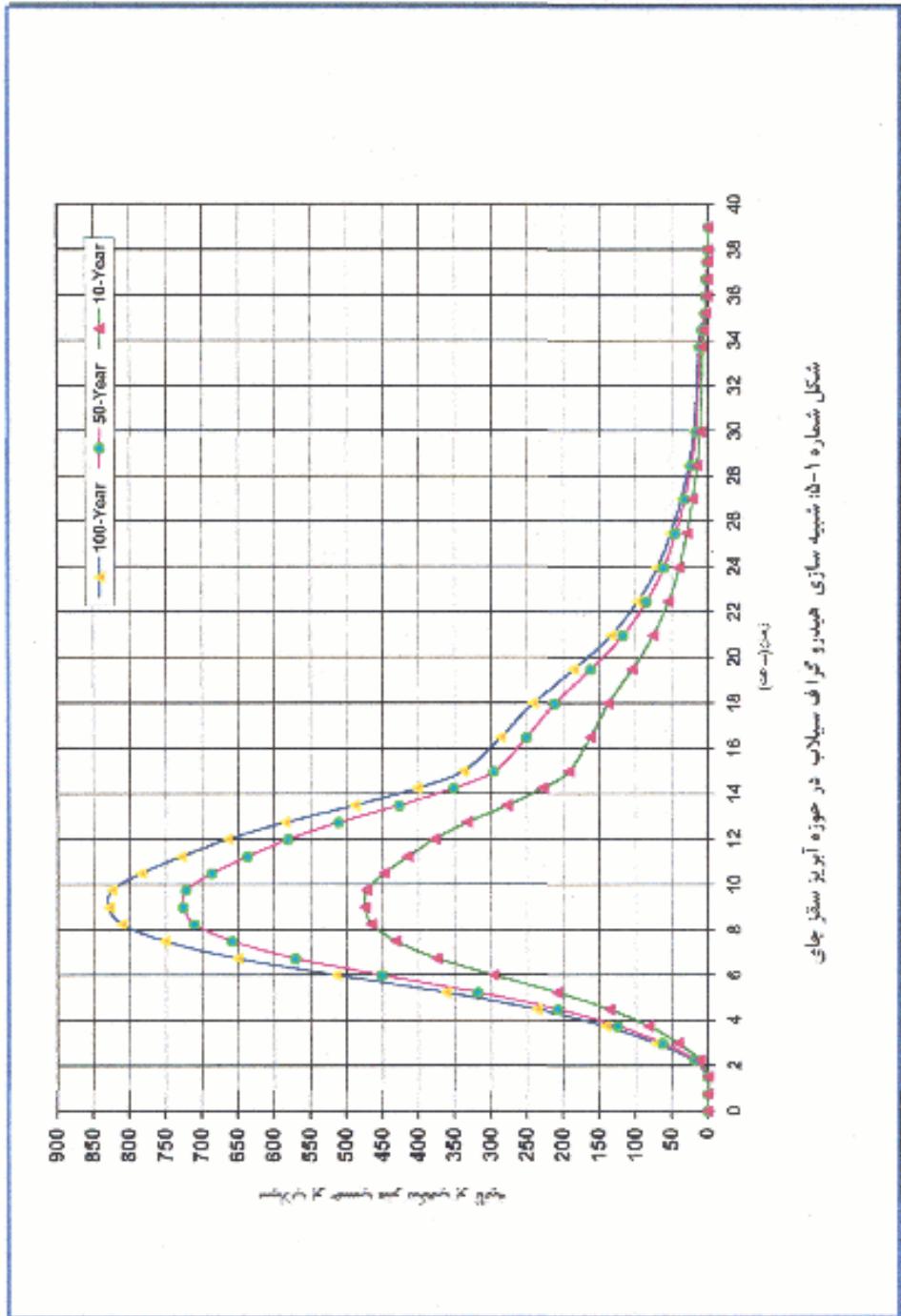
( )

Ha:u = uo

( )

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U/rp	q/rp	Wrp/rp	qhp/rp	Ratio	Hour_6	S	Q	Hour_1	Hour_2	Hour_3	Hour_4	Hour_5	Hour_6	Flood-hyd			
0.00	0.0000	0.0000	0.0000											0.00			
0.10	0.0300	0.7449	0.9966	0.0478	2.210	5.701	0.091	0.09						0.09			
0.20	0.1000	1.4986	3.3145	0.0720	3.330	0.460	0.30	0.46						0.76			
0.30	0.1800	2.247	6.299	0.5430	25.120	16.916	0.57	1.62	18.81					20.91			
0.40	0.310	2.996	10.277	0.2179	10.080	5.116	0.93	2.90	62.71	5.09				71.63			
0.50	0.470	3.746	15.581	0.0720	3.330	0.480	1.42	4.73	119.15	16.96	0.46			142.71			
0.60	0.660	4.495	21.880	0.0471	2.180	0.085	1.99	7.16	194.40	32.23	1.52	0.08		237.39			
0.70	0.820	5.244	27.185					2.47	10.06	294.74	52.58	2.90	0.28		363.03		
0.80	0.930	5.983	30.831					2.80	12.50	413.89	73.72	4.73	0.53		514.17		
0.90	0.980	6.742	32.820					2.98	14.18	514.23	111.95	7.16	0.87		651.37		
1.00	1.000	7.481	33.152					3.02	15.09	653.21	139.08	10.06	1.32		751.76		
1.10	0.990	8.240	32.820					2.99	15.24	620.84	157.74	12.50	1.85		811.16		
1.20	0.930	8.948	30.831					2.80	15.09	627.11	167.92	14.18	2.30		629.40		
1.30	0.860	9.738	28.511					2.59	14.18	620.84	165.62	15.09	2.61		824.92		
1.40	0.780	10.488	26.859					2.35	13.11	663.21	167.92	15.24	2.77		784.61		
1.50	0.680	11.237	22.543					2.05	11.89	659.31	157.74	15.06	2.80		728.89		
1.60	0.580	11.986	18.666					1.69	10.37	489.14	145.87	14.18	2.77		664.37		
1.70	0.480	12.735	15.250					1.39	8.54	426.43	132.30	13.11	2.61		584.37		
1.80	0.390	13.484	12.929					1.18	7.01	351.18	115.94	11.09	2.41		489.01		
1.90	0.330	14.233	10.940					1.00	5.95	268.47	94.98	10.37	2.19		402.95		
2.00	0.280	14.982	9.263					0.84	5.03	244.57	76.02	8.54	1.91		338.91		
2.20	0.207	16.480	6.862					0.62	4.27	206.95	56.15	7.01	1.57		288.57		
2.40	0.147	17.979	4.873					0.44	3.16	176.69	55.97	6.95	1.29		242.40		
2.60	0.107	19.477	3.547					0.32	2.24	129.81	47.49	6.03	1.09		186.99		
2.80	0.077	20.975	2.553					0.23	1.83	92.18	35.11	4.27	0.92		134.35		
3.00	0.056	22.473	1.887					0.17	1.17	67.10	24.93	3.16	0.78		97.32		
3.20	0.040	23.972	1.326					0.12	0.85	48.29	18.15	2.24	0.58		70.23		
3.40	0.029	25.470	0.961					0.09	0.61	35.12	13.08	1.63	0.41		50.92		
3.60	0.021	26.968	0.696					0.06	0.44	25.08	9.50	1.17	0.30		36.56		
3.80	0.015	28.466	0.487					0.05	0.32	18.19	6.78	0.85	0.22		25.41		
4.00	0.011	29.865	0.365					0.03	0.23	13.17	4.92	0.61	0.16		19.12		
4.50	0.005	33.710	0.166					0.02	0.17	9.41	3.56	0.44	0.11		13.71		
4.60	0.004	34.459	0.133					0.01	0.08	6.90	2.54	0.32	0.08		9.93		
4.70	0.003	35.208	0.099					0.01	0.08	3.14	1.67	0.23	0.06		6.38		
4.80	0.002	35.957	0.086					0.05	0.21	0.85	0.17	0.04	0.04		3.81		
4.90	0.001	36.707	0.033						1.88	0.68	0.08	0.03		2.67			
5.00	0.000	37.456	0.000						0.51	0.06	0.01	0.01		0.58			
		0.000	0.000							0.05	0.06	0.05	0.05		0.01		



شکل شماره ۱-۳: شبیه سازی هیدرولوژیک سیلاب در حوزه آبریز سقز جانی

Y =

SCS

X =

(CN)

$$y_A = 0.0002 x^2 + 0.533x + 84.919 \quad ( )$$

$$y_B = -0.0013 x^2 - 0.1608 x + 85.624 \quad ( )$$

$$y_C = -0.0004 x^2 - 0.1545 x + 90.555 \quad ( )$$

$$y_D = -0.00005 x^2 - 0.098 x + 91.076 \quad ( )$$

CN

Y =

CN

X =

$$CN_0 \quad C=0 \quad F=1 \\ (CN_0=CN=0) \quad CN$$

$$C=1 \quad CN=$$

P

CN

CN

C

$\lambda \quad P \quad CN$

)

$$d\lambda / \lambda \quad dP/P \quad dCN/CN \quad (dc/c$$

C Q

CN

(CN)

$\lambda$

CN P

SCS(NRCS)

CN

$$y_A = -0.0112 x^2 + 0.7911 x - 0.2096 \quad ( )$$

$$y_B = -0.0063 x^2 + 0.4453 x - 0.11 \quad ( )$$

$$y_C = -0.004 x^2 + 0.2842 x - 0.2096 \quad ( )$$

$$y_D = -0.0022 x^2 + 0.1538 x - 0.0408 \quad ( )$$

SCS

DAFI

VBA

CN

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CN

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SCS

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 \end{array}$$

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## **Abstract**

This research deal with a new method of harmonic data application of environmental resource from research area and input function, i.e. rainfall and floods as a operating agents of basin system, to obtain a model for estimation of flooding potential of basins. Serious consideration paid to understand relations between environmental factors and effects of input resource such as rainfall. In this relation applied model made it possible to determine area with iso flooding potential in region under consideration. Although using mathematical and statistical methods can answer to many questions in this field, but what makes it different is that, environmental factors and their complicated relations and their contribution to flood production in path with storms are treated from different point of view. Multiple environmental data analyzed and led moving from pure statistical definition of flood phenomenon to quantity and quality description of flood process to obtain special indexes according to available standards. This process led to obtaining applicable and fundamental results in methods for water resource development works.

Results of obtained model could predict response of iso potential sites to deferent storms.

1-Results and achievements of model can be described as follow.

1-1-Precise understanding of operation system's response to deferent systems in micro conditions (Iso potential units) and macro condition (hydrologic units) as a new method in flood process understanding.

1-2-Main specification of model and its application is estimation of CN and depth of runoff in area under consideration.

1-3-Determination of CN could be possible with introducing of mathematical equations without referring to related tables and graphs.

1-3-1-Introducing of four equations in relation to vegetation cover and land use as a direct Parameter in estimation of CN in deferent hydrologic soil condition of research area.

1-3-2- Introducing of four equations in relation to slope as an independent variable related to vegetation cover conditions on four deferent hydrologic conditions of research area.

1-4-Analysis of soils' curve numbers in four deferent conditions on 855 Iso flood potential units.

1-5-Flood hydrograph simulation on hydrologic units and Saghez Chay basin.

2-Applied results of model

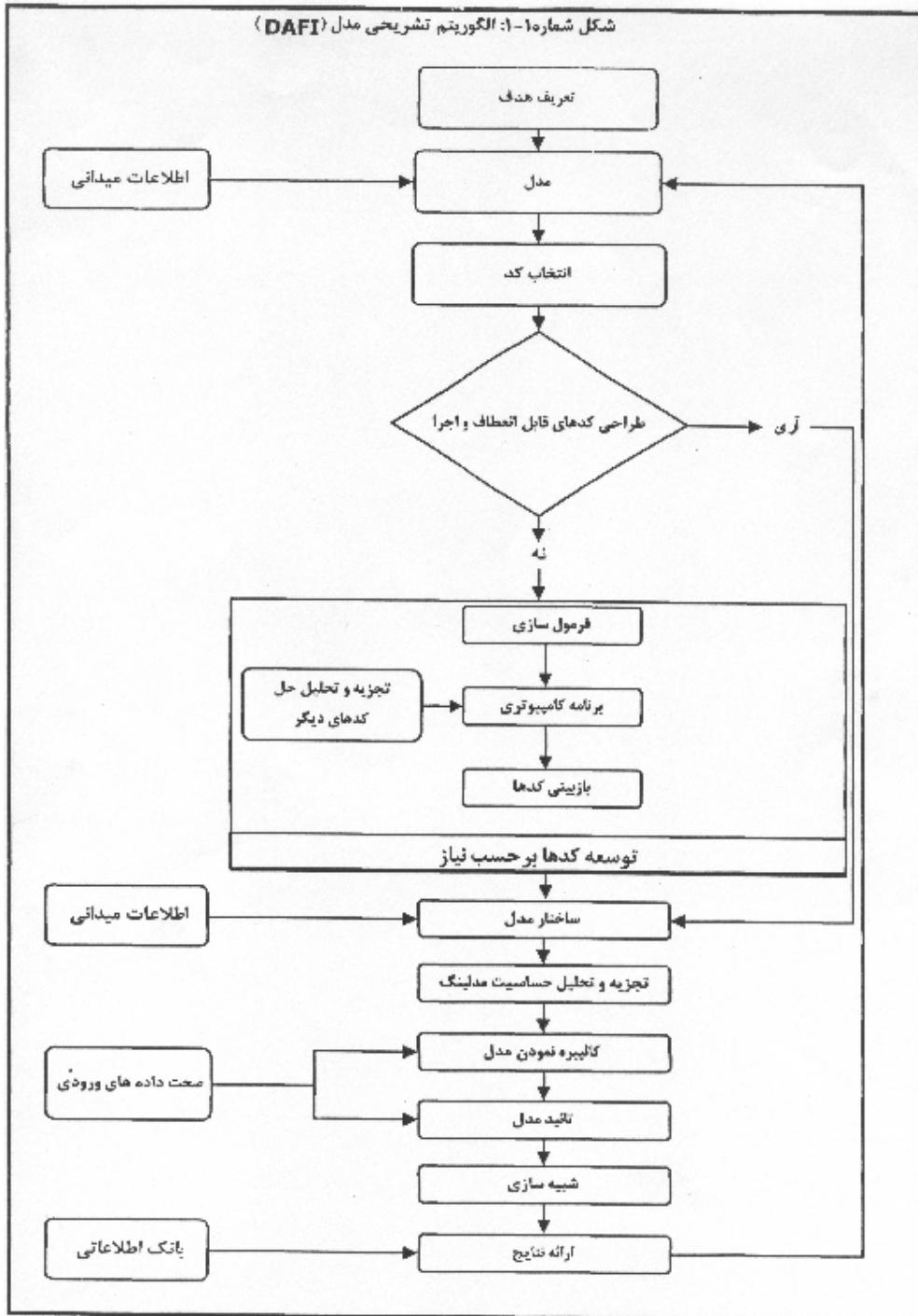
2-1-Development and generalization of SCS method for its improvement in relation to précising and fastening of CN formulation in four deferent conditions.

2-2-Strategic results of this research could be applied to improve sustainable management of water resource and evaluation of environmental resource and determination of flood potential at any time.

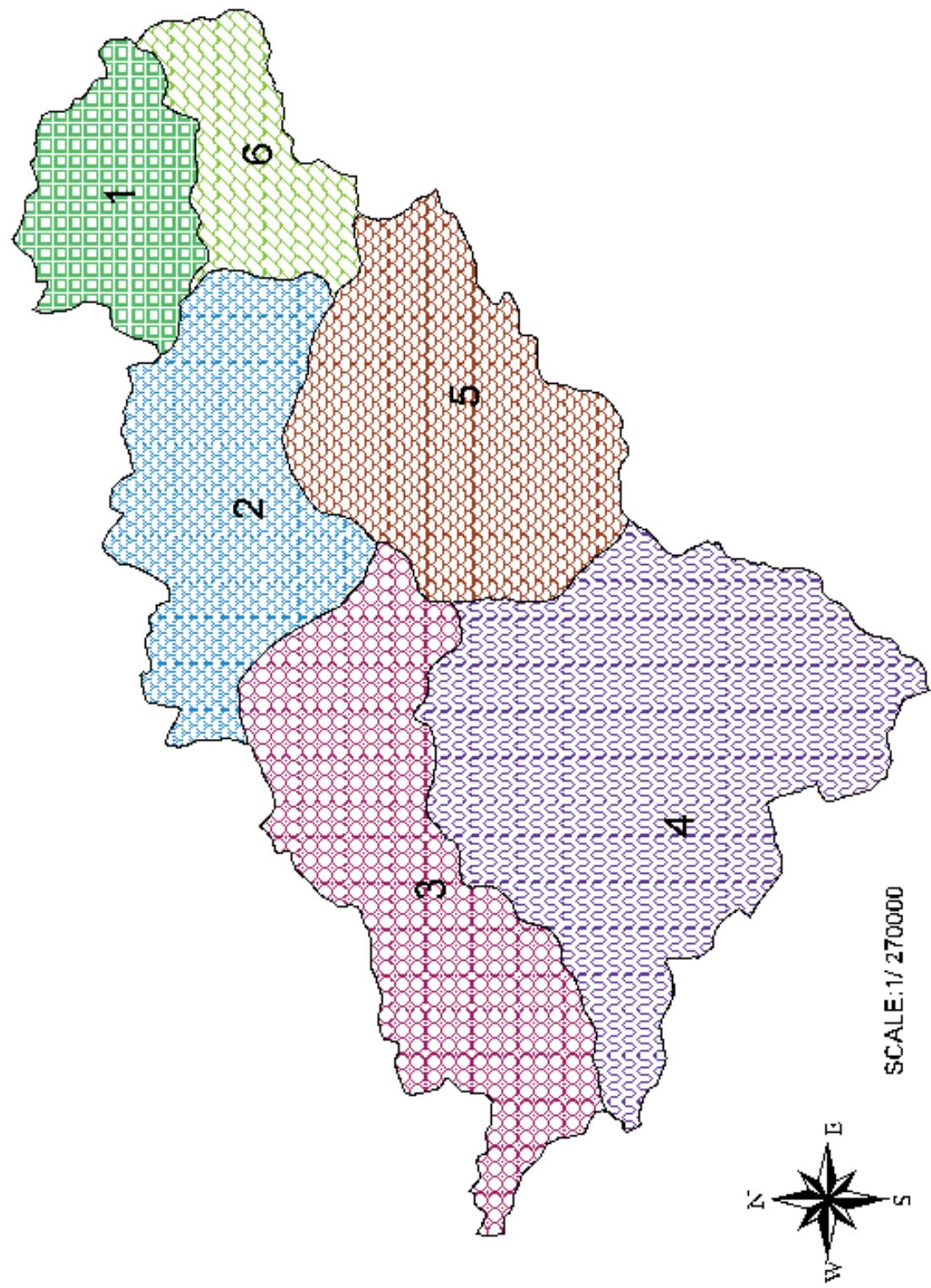
For obtaining of research aims, many different software and programming in usual basic environment are used for determination of regions flooding intensity model (DAFD)s

**Keywords:** Operating System (Basin), Input Function, Output Function, Environmental Resources, Sensitivity of Analysis Model, Calibration Model, Flooding Intensity, Development of Curve Number Method .

شکل شماره ۱: الگوریتم تشریعی مدل (DAFI)



نقشه شماره ۲: واحدهای هیدرولوژیک حوزه آبریز سفتر جای



نقشه شهرداری پیشینی شعبه های پوششی شهرستان خوی در سطح جنگل



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