

Analysis and Determination of Equivalent circuit of E-plane Metallic Strip in Rectangular Waveguides

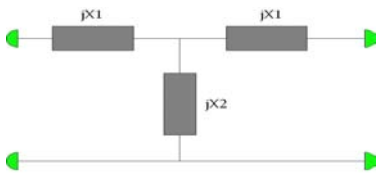
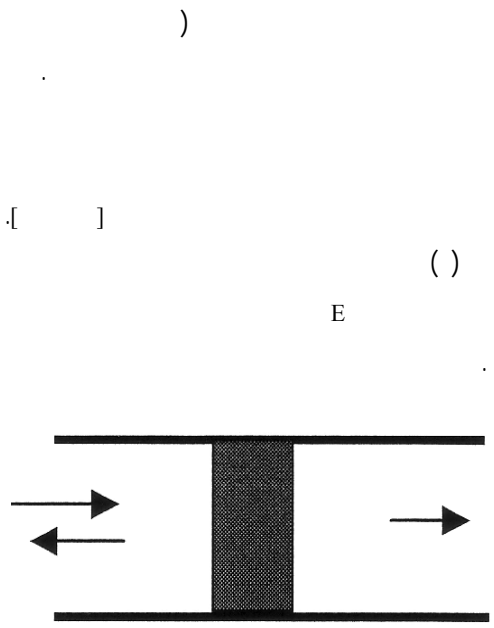
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Abstract

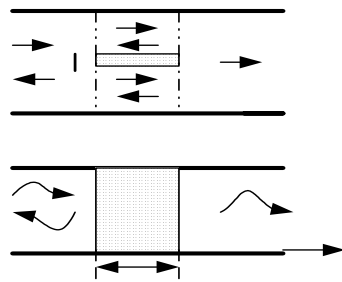
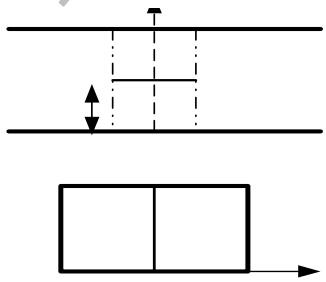
Discontinuities are used to produce impedance and transfer functions in microwave devices. Various types of filters, phase shifters, mixers and high frequency oscillators may employ some kind of discontinuity. The longitudinal E-plane metallic strip is the main part of pure metal insert (PMI) and fin-line filters. In this paper, the least squares boundary residual method (LSBRM) is employed as an effective procedure for the analysis of longitudinal E-plane thick and thin metallic strips inside waveguides. The fields inside every section of the waveguide are expanded in terms of modal functions. Then, the boundary conditions on the tangential electric and magnetic fields over the waveguide interfaces (together with a weighting factor) are used to construct an error function. The minimization of the error function determines the amplitude of the excited modes and finally the equivalent circuit of the metallic strip. The numerical results obtained by the computer simulation agree very well with those derived by other methods, in cases available in the literature. The present method is effectively employed for the design of microwave band pass filters.

Key words: Discontinuity, E-plane fin, LSBRM, Mode matching, Modal expansion, Waveguide filter.



E

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$$\bar{F} = \hat{u}_z \Phi^h, \quad \bar{A} = 0 \quad (1)$$

$$\bar{E} = -\nabla \times \bar{F}, \quad \bar{H} = -\hat{y} \bar{F} + \frac{1}{z} \nabla(\nabla \cdot \bar{F}) \quad (2)$$

$\bar{A} = \hat{u}_z \Phi^e$

$\bar{F} = \sqrt{\alpha} \sin(\frac{\pi}{a} x) e^{-j\beta_{10} z}$

$\bar{H} = -\hat{y} \bar{F} + \frac{1}{z} \nabla(\nabla \cdot \bar{F})$

$\bar{E} = -\nabla \times \bar{F}$

TE_{10}^z

$$E_y^{(i)} = \sin(\frac{\pi}{a} x) e^{-j\beta_{10} z} \quad (3)$$

$$H_x^{(i)} = \frac{-\beta_{10}}{\omega \mu} \sin(\frac{\pi}{a} x) e^{-j\beta_{10} z} \quad (4)$$

$$\beta_{10}^2 = k^2 - (\frac{\pi}{a})^2$$

$$H = E \quad (5)$$

$$\nabla^2 \Phi^h + k^2 \Phi^h = 0 \quad (6)$$

$$\hat{z} = j\omega \mu$$

$$k = \sqrt{-\hat{z} \hat{y}}$$

$$\hat{y} = j\omega \epsilon$$

$$(z) TE^z \quad \Phi^h$$

$$E_y|_{x=0,a} = 0, \quad E_x|_{y=0,b} = 0 \quad (7)$$

$$TE^z \quad (8)$$

$$[1] \quad (9)$$

$$TE^z \quad ()$$

$$\Phi_{lmn}^{Ih} = A_{lmn}^- \cos(\alpha_n y) \cdot \cos(k_{mx}^I x) \cdot e^{j\beta_{mn} \left(z + \frac{w}{2}\right)} \quad ()$$

$$\Phi_{rs}^{IIIh} = \cos(k_{rx}^{III} (x - x_1)) \cdot \cos(\alpha_s y) \cdot \left[C_{1rs}^- e^{j\beta_{rs}^{III} z} + C_{1rs}^+ e^{-j\beta_{rs}^{III} z} \right] \quad ()$$

TM^z

$$E_y^I = \frac{\partial}{\partial x} \Phi^{Ih} \quad ()$$

IV

$$H_x^I = \frac{1}{\hat{z}_1} \frac{\partial}{\partial z} E_y^I \quad ()$$

$$\Phi_{tv}^{IVh} = D_{1tv}^+ \cos(\alpha_v y) \cdot \cos(K_{tx}^{IV} x) \cdot e^{-j\beta_{tv} \left(z - \frac{w}{2}\right)} \quad ()$$

$$\alpha_n = \frac{n\pi}{b} \quad K_{mx}^I = \frac{m\pi}{a}$$

$$K_{tx}^{IV} = \frac{t\pi}{a}$$

$$\Phi_{mn}^{Ie} = (A_{1mn}^-)' \sin(K_{mx}^I x) \cdot \sin(\alpha_n y) \cdot e^{j\beta_{mn} \left(z + \frac{w}{2}\right)} \quad ()$$

$$(\alpha_{L2}^u)^2 + (\beta_{L1L2}^u)^2 = K^2 - (K_{L1x}^u)^2 \quad ()$$

$$K = \omega \sqrt{\mu \epsilon}$$

II

$$TE^z \quad ()$$

$$u = I, II, III, IV$$

$$L_1 = m, p, r, t \quad , \quad L_2 = n, q, s, v$$

$$\Phi_{pq}^{IIh} = \cos(K_{px}^{II} x) \cdot \cos(\alpha_q y) \cdot \left[B_{1pq}^- e^{j\beta_{pq}^{II} z} + B_{1pq}^+ e^{-j\beta_{pq}^{II} z} \right] \quad ()$$

$$TE_{m0}^z$$

$$TE_{10}^z$$

$$\alpha_q = \frac{q\pi}{b} \quad k_{px}^{II} = \frac{p\pi}{x_1}$$

$$() \quad ()$$

$$TM^z$$

III

$$H_x \quad E_y$$

$$: \quad Z = -W/2 \quad W/2$$

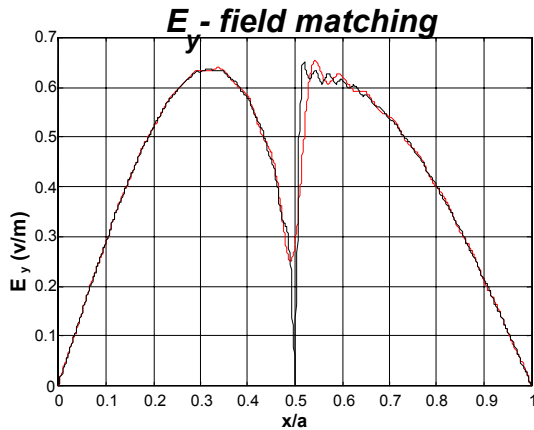
$$\begin{aligned}
 & \left(\begin{array}{c} L \\ \vdots \\ L_{8.1} \end{array} \right) \bar{F} \quad T \\
 & \left(\begin{array}{c} L_{1.1} \quad \dots \quad L_{1.6} \\ \vdots \quad \vdots \quad \vdots \\ L_{8.1} \quad \dots \quad L_{8.6} \end{array} \right)_{8 \times 6} \left(\begin{array}{c} \vdots \\ \vdots \\ \vdots \end{array} \right)_{6 \times 1} = \left(\begin{array}{c} \vdots \\ \vdots \\ \vdots \end{array} \right)_{8 \times 1} \quad () \\
 & \left(\sum_m E_y^I + E_y^{(i)} \right) \Big|_{Z=w/2} = \left(\sum_t E_y^{II} \right) \Big|_{Z=-w/2} \quad () \\
 & \left(\sum_m H_x^I + H_x^{(i)} \right) \Big|_{Z=w/2} = \left(\sum_t E_x^{II} \right) \Big|_{Z=-w/2} \quad ()
 \end{aligned}$$

$$\begin{aligned}
 & IV, III, II, I \quad N, Q, P, M \\
 & (8) \times (M+2P+2Q+N) \quad L \\
 & 0 \leq x \leq x_1 \quad () \quad () \\
 & 0 \leq y \leq b \quad x_1 \leq x \leq a \\
 & S3 \quad 0 \leq y \leq b \\
 & S4 \quad 0 \leq y \leq b
 \end{aligned}$$

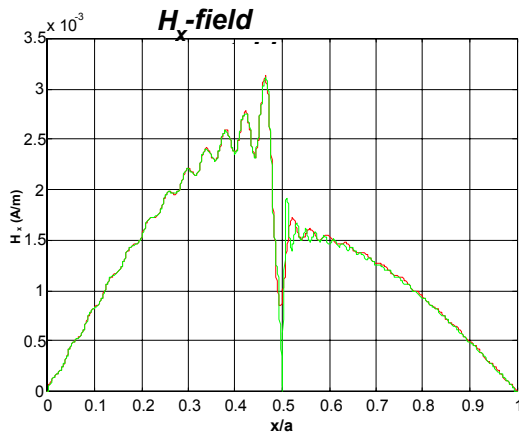
$$\begin{aligned}
 & \left(\begin{array}{c} \vdots \\ \vdots \\ \vdots \end{array} \right) \quad \varepsilon \quad (LSBRM) \\
 & \bar{u} = L\bar{V} - \bar{F} \quad () \\
 & \langle \bar{u}^*, \bar{u} \rangle = \int_{B.S.} \bar{u}^* \bar{u} \, ds \quad () \\
 & \varepsilon = \langle (L\bar{V} - \bar{F})^*, (L\bar{V} - \bar{F}) \rangle \quad () \\
 &) \bar{V} \quad \varepsilon \quad () \quad () \\
 & () \quad (\bar{V}^* \quad 0 \leq y \leq b \quad c \leq x \leq c+t \quad ()
 \end{aligned}$$

$$\begin{aligned}
 & \bar{V}_{min} = \langle L^*, L \rangle^{-1} \cdot \langle L^*, \bar{F} \rangle \quad () \\
 & \bar{F} \quad L \\
 & \langle L^*, \bar{F} \rangle \quad \langle L^*, L \rangle \quad () \\
 & \left(\sum_{ln} E_y^I + E_y^{(i)} \right) \Big|_{Z=-w/2} = 0 \quad () \\
 & \left(\sum_n E_y^{IV} \right) \Big|_{Z=w/2} = 0 \quad ()
 \end{aligned}$$

$$\begin{aligned}
 & (S_i) \quad L \\
 & \langle L^*, L \rangle, \langle L^*, \bar{F} \rangle \quad [] () \\
 & L\bar{V} = \bar{F} \quad () \\
 & \bar{V} = [A_m^-, B_p^+, B_p^-, C_q^+, C_q^-, D_n^+]^T \quad ()
 \end{aligned}$$



() - a



() - b

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X
 $b = 0.4(\text{inch}) \quad a = 0.9(\text{inch})$
 () b w
 () $x_1 = c$
 () (t)

T

()

$$\langle L^*, L \rangle_{1,1} = \left(1 + \frac{\alpha}{Z_{1r}^* Z_{1m}}\right) \cdot \left[\int_{S=S_1+S_2} \Phi_r^{I*}(x,y) \cdot \Phi_m^I(x,y) ds \right]$$

$$\langle L^*, L \rangle_{2,1} = -\left(1 - \frac{\alpha}{Z_{1r}^* Z_{2m}}\right) \cdot \left[\int_{S_1} e^{j\frac{PO^2}{2}} \cdot \Phi_r^{I*}(x,y) \cdot \Phi_p^{II}(x,y) ds \right]$$

()

$$\Phi_{L1}^u(x,y)$$

()

$$() (\bar{V})$$

$$A_1^-$$

$$[] A_1^+ = 1$$

$$\bar{Y}_{in} = \frac{1-\Gamma}{1+\Gamma} = \frac{1-A_1^-}{1+A_1^-} \quad ()$$

$$() \quad T \quad E \quad ()$$

$$\bar{Y}_{in} = G_{in} + jB_{in} \quad ()$$

$$\bar{Y}_{in} \quad X_2 \quad X_1 \quad () \quad () \quad ()$$

$$X_1 = \mp X_2 + \frac{B_{in}}{G_{in} - (B_{in}^2 + G_{in}^2)} \quad ()$$

$$X_2 = \pm [(X_1 \pm X_2)^2] + \frac{G_{in} - 1}{B_{in}^2 + G_{in}^2 - G_{in}} \quad ()$$

(c = a/2)

((a,b . .))

[]

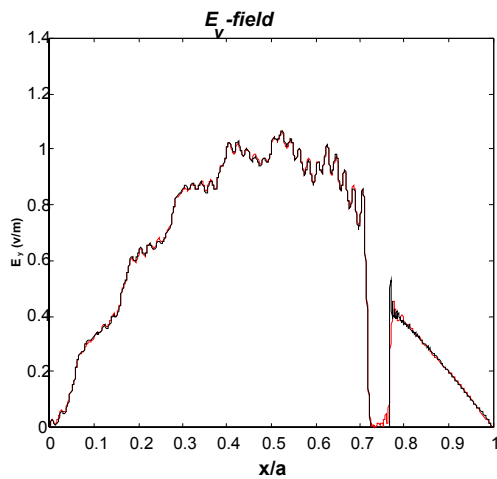
[]

(b)

)

(

< L*, L >



() α

()

(a,b)

H, E

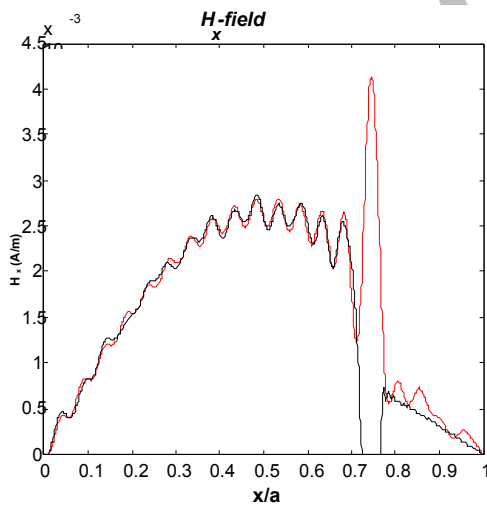
a

()

- a

(M = N = P = Q = 20)

(a,b)



()

Q = 50 P = 60 M = N = 40

(t/a = 0.05)

x1/a = 0.725

H, E

()

- b

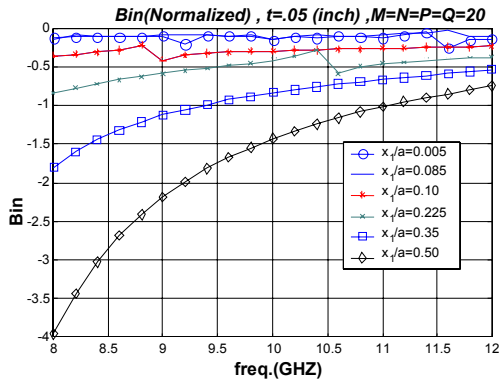
[]

(a)

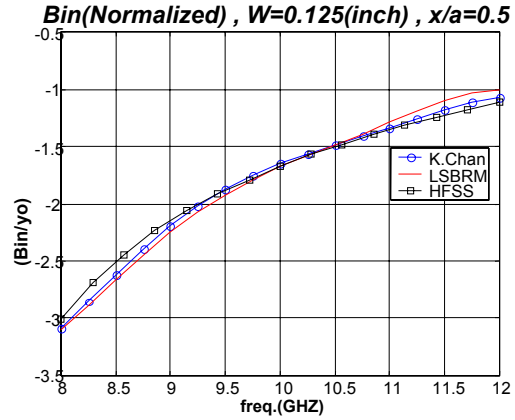
TE_{m0}^z

(b)

(a) ((b) . .)



- b



- a

M=N=P=Q=20

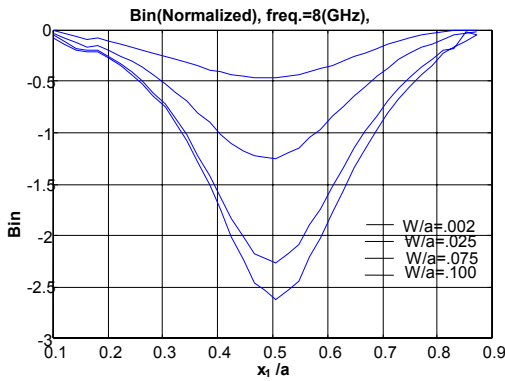
W=.15 (inch)

M=N=P=Q=30 c=a/2

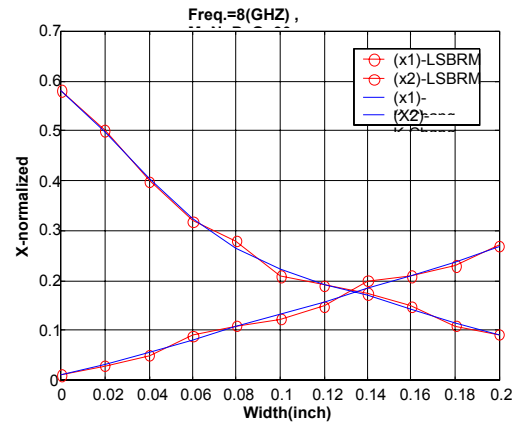
(b) (a)

(W)

x1



- a



(x2) (x1)

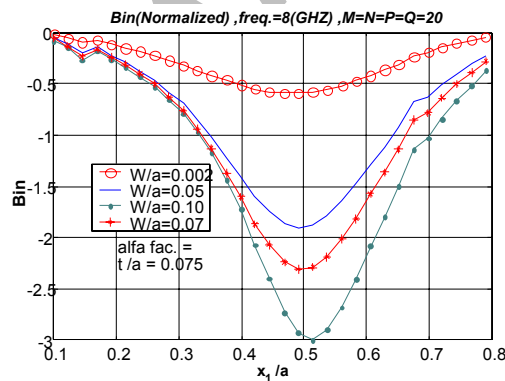
- b

freq.=8(GHZ) c=a/2

M=N=P=Q=30

freq.=8(GHZ) M=N=P=Q=20

X1

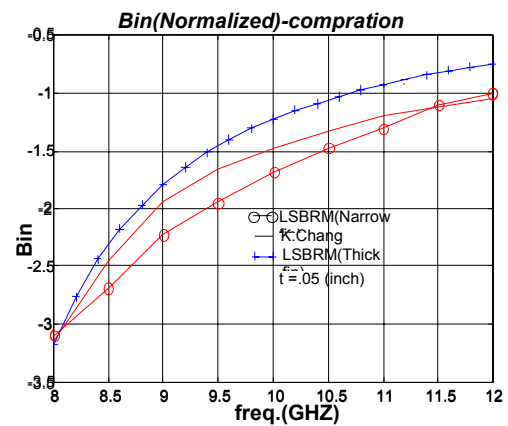


- b

M=N=P=Q=20

Freq.=8(GHZ)

X1

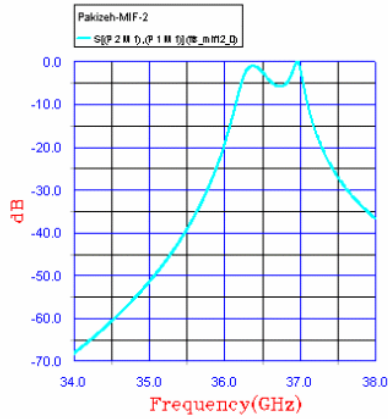


- a

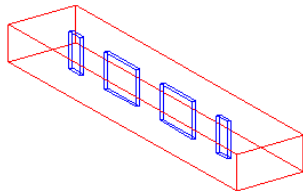
W=.125 (inch) M=N=P=Q=2 c=a/2

HFSS

(a)



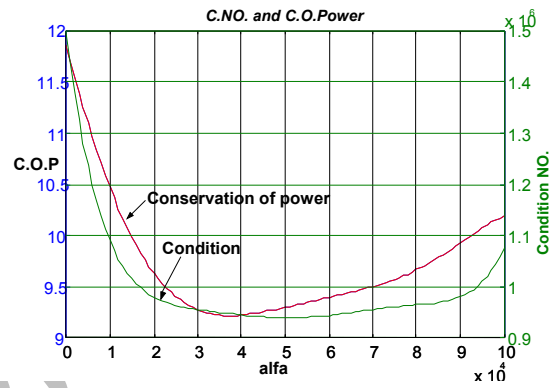
PMI S21 - a
 : ka x1=a/2 t=0.35(mm)
 (HFSS) .b=3.556(mm) a=7.112(mm)



PMI - b
 : ka x1=a/2 t=0.35(mm)
 b=3.556(mm) a=7.112(mm)

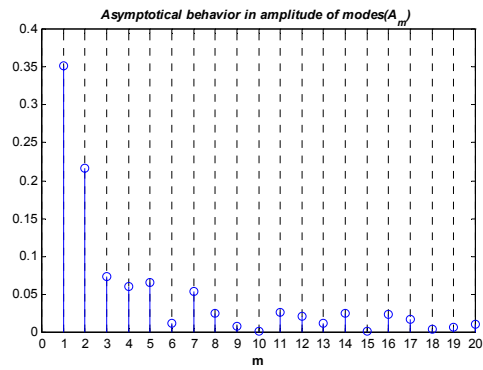
E

(b) (A)I (TE)



- a

x1=0.45(inch)
 M=N=P=Q=30



- b

x1=0.3(inch) t/a=0.05 (A)
 M=N=P=Q=20

64MB, P.II

()

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Bin (), $t=0.05$ () $M=N=P=Q=20$
(GHZ)

Bin (), $=8$ (GHZ), $M=N=P=Q=20$

Bin (), () $=8$ (GHZ), $M=N=P=Q=20$

E-

H-

E-

H-

Bin () $W=0.125$ (inch), $x/a=0.5$
(GHZ)

$=8$ (GHZ), $M=N=P=Q=30$

()

Bin () - , $M=N=P=Q=20$
(GHZ)

